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An overview of wind energy-status 2002

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Abstract

The paper provides an overview of the historical development of wind energy technology and discusses the current world-wide status of grid-connected as well as stand-alone wind power generation. During the last decade of the twentieth century, grid-connected world-wide wind capacity has doubled approximately every three years. Due to the fast market development, wind turbine technology has experienced an important evolution over time. An overview of the different design approaches is given and issues like power grid integration, economics, environmental impact and special system applications, such as offshore wind energy, are discussed. Due to the complexity of the wind energy technology, however, this paper mainly aims at presenting a brief overview of the relevant wind turbine and wind project issues. Therefore, detailed information to further readings and related organisations is provided. This paper is an updated version of the article ‘*Wind Energy Technology and Current Status: A Review*’, published in *Renewable and Sustainable Energy Reviews*, 4/2000, pp. 315–374. This update was requested by Elsevier due to the large interest in wind power. © 2002 Elsevier Science Ltd. All rights reserved.

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1. Introduction

The power of the wind has been utilised for at least three thousand years. Until the early twentieth century wind power was used to provide mechanical power to pump water or to grind grain. At the beginning of modern industrialisation, the use of the fluctuating wind energy resource was substituted by fossil fuel fired engines or the electrical grid, which provided a more consistent power source.

In the early 1970s, with the first oil price shock, the interest in the power of the wind re-emerged. This time, however, the main focus was on wind power providing electrical energy instead of mechanical energy. This way, it became possible to provide a reliable and consistent power source by using other energy technologies—via the electrical grid—as a back-up.

The first wind turbines for electricity generation had already been developed at the beginning of the twentieth century. The technology was improved step by step since the early 1970s. By the end of the 1990s, wind energy has re-emerged as one of the most important sustainable energy resources. During the last decade of the twentieth century, world-wide wind capacity has doubled approximately every three years. Costs of electricity from wind power has fallen to about one-sixth since the early 1980s. And the trend seems to continue. Some experts predict that the cumulative capacity will be growing world-wide by about 25% per year until 2005 and cost will be dropping by an additional 20 to 40% during the same time period [8], vol. 15, no. 5, p. 8.

Wind energy technology itself also moved very fast towards new dimensions. At the end of 1989, a 300 kW wind turbine with a 30-meter rotor diameter was the state of the art. Only 10 years later, 1500 kW turbines with a rotor diameter of around 70 meters are available from many manufacturers. The first demonstration projects using 2 MW wind turbines with a rotor diameter of 74 meters were installed before the turn of the century. 2 MW turbines are now commercially available and 4 to 5 MW wind turbines are currently under development. First prototypes will be installed in 2002 (see also Table 1).

This fast development of the wind energy market as well as of the technology has large implications on research and education as well as on professionals working

Table 1
Development of wind turbine size between 1985 and 2000^a

Year	Capacity	Rotor Diameter
1985	50 kW	15 m
1989	300 kW	30 m
1992	500 kW	37 m
1994	600 kW	46 m
1998	1500 kW	70 m
2002 ^b	3500–4500 kW	88–112 m

^a Source: DEWI [24].

^b Figures for the year 2002 are estimated, based on information published in [8].

for electric utilities or the wind energy industry. It is important to mention that more than 83% of the world-wide wind capacity is installed in only five countries: Germany, USA, Denmark, India and Spain. Hence, most of the wind energy knowledge is based in these countries. The use of wind energy technology, however, is fast spreading to other areas in the world. Hence, the available information must also be spread around the world. That is the main purpose of this review paper. But despite the fact that wind energy has already been utilised for three thousand years, it is a very complex technology. The technology involves technical disciplines such as aerodynamics, structure-dynamics, and mechanical as well as electrical engineering. Due to the complexity of the wind energy technology this wind energy review paper is not able to cover all related topics in great detail. The paper aims rather at presenting an overview of the relevant areas as well as providing links to further readings and related organisations.

The content of the paper is as follows: Section 2 provides a brief overview of the historical development, and Section 3 presents the current status; Section 4 introduces the physical background of utilising the energy in the wind; Section 5 discusses different wind turbine designs; Section 6 deals with the integration of wind energy into the electrical network; Section 7 provides some information about wind energy economics, and Section 8 with issues related to the installation and the design of wind energy projects; Section 9 presents special system applications and Section 10 will present some thoughts about the future of wind power generation. Section 11 lists many of the associations, research organisations and conferences dealing with wind energy. Section 12 highlights some of the information contained in the list of references.

2. Historical background

The historical development of wind turbine technology is documented in many publications. The following section will therefore provide only a very brief overview

of the development. References for this chapter: [33], pp. 118–130; [30], pp. 9–19; [55], p. 7; but also [31, 47, 21, 46, 65, 61, 75, 51, 53, 37, 172, 60, 52, 7, 20, 25].

2.1. Mechanical power generation

The earliest windmills recorded are vertical-axis mills. These wind mills can be described as simple drag devices. These windmills have been used in the Afghan highlands to grind grain since the seventh century BC.

The first details about horizontal-axis windmills are found in historical documents from Persia, Tibet and China at about 1000 AD. This windmill type has a horizontal shaft and blades (or sails) revolving in the vertical plane. From Persia and the Middle East, the horizontal-axis windmill spread across the Mediterranean countries and Central Europe. The first horizontal-axis windmill appeared in England around 1150, in France 1180, in Flanders 1190, in Germany 1222 and in Denmark 1259. This fast development was most likely influenced by the Crusaders, taking the knowledge about windmills from Persia to many places in Europe.

In Europe, windmill performance was constantly improved between the twelfth and nineteenth centuries. By the end of the nineteenth century, the typical European windmill used a rotor 25 meters in diameter and the stocks reached up to 30 meters. Windmills were not only used for grinding grain, but also for pumping water to drain lakes and marshes. By 1800, about 20,000 modern European windmills were in operation in France alone. And in the Netherlands, 90% of the power used in industry was based on wind energy. Industrialisation then led to a gradual decline in windmills, but even in 1904 wind energy provided 11% of the Dutch industry energy and Germany had more than 18,000 units installed.

By the time when the European windmills slowly started to disappear, windmills were introduced by settlers in North America. Small windmills for water pumping to water livestock became very popular. These windmills, also known as American windmills, operated fully self-regulated, hence they could be left unattended. The self-regulating mechanism pointed the rotor windward during high wind speeds. The European-style windmills usually had to be turned out of the wind or the sailing blades had to be rolled up during extreme wind speeds to avoid damage to the windmill. The popularity of windmills in the US reached its peak between 1920 and 1930 with about 600,000 units installed. Various types of American windmills are still used for agricultural purposes all over the world.

2.2. Electrical power generation

In 1891, the Dane Poul LaCour was the first to build a wind turbine generating electricity. Danish engineers improved the technology during World Wars I and II and used the technology to overcome energy shortages. The wind turbines by the Danish company F.L. Smidth built in 1941/42 can be considered as forerunners of modern wind turbine generators. The Smidth turbines were the first to use modern airfoils, based on the advancing knowledge of aerodynamics at this time. At the same time, the American Palmer Putnam built a giant wind turbine for the American

company Morgan Smith Co., with a diameter of 53 meters. Not only the size of this machine was significantly different, but also the design philosophy. The Danish philosophy was based on an upwind rotor with stall regulation, operating at slow speed. Putnam's design was based on a downwind rotor with a variable pitch regulation. Putnam's turbine, however, was not very successful. It was dismantled in 1945 [33]. See Table 2 for an overview of important historical wind turbines.

After World War II, Johannes Juul in Denmark developed the Danish design philosophy further. His turbine installed in Gedser, Denmark, generated about 2.2 million kWh between 1956 and 1967. At the same time, the German Hütter developed a new approach. His wind turbine comprised two slender fibreglass blades mounted downwind of the tower on a teetering hub. Hütter's turbine became known for its high efficiency [33, 25]/.

Despite the early success of Juul's and Hütter's wind turbines, the interest in large-scale wind power generation declined after World War II. Only small-scale wind turbines, for remote area power systems or for battery charging, received some interest. With the oil crises in the beginning of the 1970s, the interest in wind power generation returned. As a result, financial support for research and development of wind energy became available. Countries like Germany, USA and Sweden used this money to develop large-scale wind turbine prototypes in the MW range. Many of these prototypes, however, did not perform very successfully most of the time (see Table 3), due to various technical problems, e.g. with the pitch mechanisms.

Nevertheless, due to special government support schemes in certain countries, e.g. Denmark, further development in the field of wind energy utilisation took place. The single most important scheme was the Public Utility Regulatory Policies Act (PURPA), passed by the US Congress in November 1978. With this Act, President

Table 2
Historical wind turbines^a

Turbine, country	Diameter (m)	Swept area (m ²)	Power (kW)	Specific power (kW/m ²)	Number of blades	Tower height (m)	Date in service
Poul LaCour, DK	23	408	18	0.04	4	-	1891
Smith-Putnam, US	53	2231	1250	0.56	2	34	1941
F.L. Smidth, DK	17	237	50	0.21	3	24	1941
F.L. Smidth, DK	24	456	70	0.15	3	24	1942
Gedser, DK	24	452	200	0.44	3	25	1957
Hutter, Germany	34	908	100	0.11	2	22	1958

^a Source: Gipe [33], p. 78.

Table 3
Performance of the first large-scale demonstration wind turbines^a

Turbine, country	Diameter [m]	Swept area [m]	Capacity [MW]	Operating hours	Generated GWh	Period
Mod-1, US	60	2,827	2	–	–	79–83
Growian, D	100	7,854	3	420	–	81–87
Smith-Putnam, US	53	2,236	1.25	695	0.2	41–45
WTS-4, US	78	4,778	4	7,200	16	82–94
Nibe A, DK	40	1,257	0.63	8,414	2	79–93
WEG LS-1, GB	60	2,827	3	8,441	6	87–92
Mod-2, US	91	6,504	2.5	8,658	15	82–88
Näsudden I, S	75	4,418	2	11,400	13	83–88
Mod-OA, US	38	1,141	0.2	13,045	1	77–82
Tjæreborg, DK	61	2,922	2	14,175	10	88–93
École, CD	64	4,000	3.6	19,000	12	87–93
Mod-5B, US	98	7,466	3.2	20,561	27	87–92
Maglarp WTS-3, S	78	4,778	3	26,159	34	82–92
Nibe B, DK	40	1,257	0.63	29,400	8	80–93
Tvind, DK	54	2,290	2	50,000	14	78–93

^a Source: Gipe [33], p. 104.

Carter and the US Congress aimed at an increase of domestic energy conservation and efficiency, and thereby decreasing the nation's dependence on foreign oil. PURPA, combined with special tax credits for renewable energy systems, led to the first wind energy boom in history. Along the mountain passes east of San Francisco and north-east of Los Angeles, huge wind farms were installed. The first of these wind farms consisted mainly of 50 kW wind turbines. Over the years, the typical wind turbine size increased to about 200 kW at the end of the 80s. Most wind turbines were imported from Denmark, where companies had further developed Poul LaCour and Johannes Juul's design philosophy of upwind wind turbines with stall regulation. At the end of the 80s, about 15,000 wind turbines with a capacity of almost 1,500 MW were installed in California.

At this time, the financial support for wind energy slowed down in the USA, but picked up in Europe and later in India. In the 90s, the European support scheme was mainly based on fix feed-in tariffs for renewable power generation. The Indian approach was mainly based on tax deduction for wind-energy investments. These support schemes led to a fast increase of wind turbine installations in some European countries, particularly in Germany, as well as in India.

Parallel to the development of the market size, also the technology developed further. By the end of the twentieth century, twenty years after the unsuccessful world-wide testing of megawatt wind turbines, the 1.5 MW wind turbines have become the technical state-of-the-art.

3. Current status

The following section will provide a brief overview of the wind energy status around the world at the end of the twentieth century. Furthermore, major wind energy support schemes will be presented. The overview is divided into grid-connected wind power generation and stand-alone systems. Finally, the overall potential of wind energy is discussed.

References for this chapter: Wind energy statistics are regularly published by various organisations. Regional or country-wide statistics are often compiled and published by the corresponding wind energy association (see Section 11.1). Also the German Wind Energy Institute as well as the International Economic Platform for Renewable Energies regularly publish world-wide statistics (see Section 11.2 for contact details). Regularly up-dated world-wide statistics are published by Wind-power Monthly [8] in the January, April, July as well as in the October edition. The Danish wind energy consultant BTM also publishes an annual wind energy development status report with world-wide statistics and forecasts. The European Wind Energy Association's publication [101] provides a very good overview of the current status as well as an interesting future scenario of how to meet 10% of the world's electricity demand with wind power by 2020, and the IEA Wind Energy Annual Report [50, 3] provides a detailed overview of the research and industry activities and policies in the area of wind energy for each IEA member state.

3.1. Overview of grid-connected wind power generation

Wind energy was the fastest growing energy technology in the 90s, in terms of percentage of yearly growth of installed capacity per technology source. The growth of wind energy, however, is not evenly distributed around the world (see Table 4). By the end of 1999, around 70% of the world-wide wind energy capacity was installed in Europe, a further 19% in North America and 9% in Asia and the Pacific.

Table 4
Operational wind power capacity world-wide^a

Region	Installed capacity [MW]		End 1999	End 2000	End 2001
	End 1995	End 1997			
Europe	2,518	4,766	9,307	12,972	16,362
North America	1,676	1,611	2,619	2,695	4,440
South & Central America	11	38	87	103	103
Asia & Pacific	626	1,149	1,403	1,795	2,162
Middle East & Africa	13	24	39	141	203
Total world-wide	4,844	7,588	13,455	17,706	23,270

^a Source: January edition 1997, 1998, 2000, 2001 and 2002 of [8].

3.1.1. Europe

Between the end of 1995 and end of 1999, around 75% of all new grid-connected wind turbines world-wide have been installed in Europe (see Tables 4 and 5). The main driver for this development was the creation of *fixed feed-in tariffs*. Such feed-in tariffs are defined by the governments as the price per kWh that the local distribution company has to pay for local renewable power generation fed into the local distribution grid (for an overview of tariffs, see [27]). Fixed feed-in tariffs reduce the risk of changing electricity prices and therefore provide a long-term secure income to investors. Feed-in tariffs exist in Germany and Spain, for instance.

In England, Scotland, as well as in Ireland, *bidding processes* are used. Thereby, potential developers of renewable energy projects are invited to submit offers for building new projects. Developers bid under different technology brands, e.g. wind or solar, for a feed-in tariff or for the amount of financial incentives to be paid for each kWh fed into the grid by renewable energy systems. The best bidder(s) will be awarded their bid feed-in tariff for a predefined period [57, 148].

Table 5
Operational wind power capacity in Europe^a

Country	Installed capacity [MW]	
	End 1995	End 2001
Germany	1,136	8,100
Denmark	619	2,417
Spain	145	3,175
Netherlands	236	483
UK	200	477
Sweden	67	264
Italy	25	560
Greece	28	273
Ireland	7	132
Portugal	13	127
Austria	3	86
Finland	7	39
France	7	87
Norway	4	16
Luxembourg	0	10
Belgium	0	18
Turkey	0	20
Czech Republic	7	12
Poland	1	16
Russia	5	5
Ukraine	1	40
Switzerland	0	3
Latvia	0	1
Romania	0	1
Total	2,518	16,362

^a Source: January edition 1997 and January edition 2002 of [8].

A new renewable energy policy was introduced in the Netherlands in February 1998. The approach is based on *fixed quotas combined with green certificate trading*. Thereby, the Government introduced fixed quotas for utilities regarding the amount of renewable energy per year they have to sell via their network. On the other hand, producers of renewable energy receive a certificate for a certain amount of energy fed into the grid. The utilities have to buy these certificates to show that they have fulfilled their obligation. Similar schemes are under discussion in other European countries, e.g. Denmark [69].

No detailed data regarding the average size of the wind turbines installed in Europe are available. Table 6 presents the development of the average size of new wind turbine installations in Germany.

The average size of the yearly installed wind turbines in Germany increased from 143 kW in 1989 to 1278 kW in 2001. In 2001, in Germany 1633 out of a total of 2079 newly installed wind turbines had a capacity of 750 kW or more. 1033 newly installed wind turbines even had a capacity of 1.5 MW or more. Due to the infrastructure required for the road transport and installation on site, e.g. cranes, the multi-megawatt wind turbines are seldom used outside Germany and Denmark. The 500 to 1000 kW range is predominant regarding the installation in the other European countries.

First offshore projects have materialised in Denmark, the Netherlands and Sweden (see Table 7). Further offshore projects are planned particularly in Denmark (Horns Rev: 150 MW; Rødsand: 150 MW), but also in Sweden (Lillgrund Bank: 48 MW), Germany (Borkum West: 60 MW), the Netherlands (Mouth of the Western Scheldt River: 100 MW; IJmuiden: 100 MW), England (see <http://www.offshorewindfarms.co.uk>) and Ireland (Kish Bank: 250+ MW; Arklow: 200+ MW).

Table 6

Average size of yearly new installed wind capacity in Germany [in kW]^a

Year	Average size of yearly new installed capacity in Germany [kW]
1988	66.9
1989	143.4
1990	164.3
1991	168.8
1992	178.6
1993	255.8
1994	370.6
1995	472.2
1996	530.5
1997	628.9
1998	785.6
1999	935.5
2000	1114
2001	1278

^a Source: German Wind Energy Institute.

Table 7
Offshore wind energy projects^a

Name	Year	Capacity [MW]	Wind speed at hub [m/s]	Hub height [m]	Distance from shore [km]	Water depth [m]	Spec. cost [ECU/kW]
Nogersund, SE	1991–98	1*0.22	–	37.5	0.25	7	–
Vindeby, Baltic Sea, DK	1991	11*0.45	7.5	37.5	1.5	3–5	~ 2150
Lely, IJsselmeer, NL	1994	4*0.5	7.7	41.5	1	5–10	~ 1700
Tunø Knob, Baltic Sea, DK	1995	10*0.5	~7.5	43	6	3–5	~ 2200
Dronen, NL	1996	28*600	–	50	30	1–2	–
Bockstigen, Baltic Sea, SE	1997	5*0.55	8	41.5	4	5–6	~ 1500
Lumijoki/ Oulu, Baltic Sea, F	1999	1*0.66	–	50	0.5	2–3	–
Utgrunden, Baltic Sea, SE	2000	7*1.425	–	65	8	7–10	~ 2070
Blyth, North Sea, UK	2000	2*2	–	58	1	5–6	~ 1600
Middelgrunden Baltic Sea, DK	2001	20*2	–	60	1–3	2–6	~ 1200
Yttre Stengrund , Baltic Sea, SE	2001	5*2	–	60	5	8	–

^a SE=Sweden, DK=Denmark, NL=The Netherlands, F=Finland. Source: [88], p. 26, <http://www.middelgrunden.dk>, <http://home.wxs.nl/~windsh/offshore.html>, and author.

Onshore, a significant increase in wind energy development is expected to take place in the near future in Spain, Turkey, France and Greece (see various editions of [8]).

3.1.2. North America

After the boom in California during the mid-1980s, development slowed down significantly in North America. In the middle of the 90s, the dismantling of old wind farms sometimes exceeded the installations of new wind turbines, which led to a reduction in installed capacity.

In 1998, a second boom started in the USA. This time, wind project developers aimed at installing projects before the federal Production Tax Credit (PTC) expired on the 30th of June 1999. The PTC added \$0.016–0.017/kWh to wind power projects for the first ten years of a wind plant's life. Between the middle of 1998 and 30th June 1999, the final day of PTC, more than 800 MW of new wind power generation were installed in the USA, which includes between 120 and 250 MW of “repowering” development at several California wind farms. A similar development took place before the end of 2001, which added 1600 MW between the middle of 2001 and the end of December 2001 (see Tables 8 and 9). Apart from Texas, major projects were carried out in the states of Minnesota, Oregon, Wyoming and Iowa. The first large-scale projects were also installed in Canada.

The typical wind turbine size installed in North America at the end of the 90s was between 500 to 1000 kW. The first megawatt turbines have also been installed in 1999 and in 2001 many projects have used megawatt turbines. In comparison to Europe, however, the overall size of wind farm projects is usually larger. Typical projects in North America are larger than 50 MW, with some projects of up to 200 MW, while in Europe projects are usually between 20 to 50 MW. The reason for this is the limited space, due to the high population density in Central Europe. These limitations led to offshore developments in Europe, but in North America offshore projects are not a major topic.

The major drivers for further wind energy development in several states in the US are an extension of the PTC as well as fixed quotas combined with green certificate trading, known in the US as Renewable Portfolio Standard (RPS). The certifi-

Table 8
Operational Wind Power Capacity in North America^a

Country	Installed capacity [MW]	
	End 1995	End 2001
USA	1,655	4,280
Canada	21	200
Total	1,676	4,440

^a Source: see Table 2.

Table 9
Operational wind power capacity in the USA by the end of 2001^a

State	Installed capacity [MW]
California	1,688
Texas	1,100
Iowa	332
Minnesota	311
Oregon	199
Washington	161
Wyoming	140
Kansas	114
Colorado	58
Wisconsin	53
Pennsylvania	34
New York	19
Hawaii	11
Vermont	6
Nebraska	3
South Dakota	3
Tennessee	2
North Dakota	2
Alaska	1
Massachusetts	1
Michigan	1
New Mexico	1
Total	4,240

^a Source: January edition 2002 of [8].

cates are called Renewable Energy Credits (RECs). Other drivers will be financial incentives, e.g. offered by the California Energy Commission (CEC), as well as green pricing programs. Green Pricing is a marketing program offered by utilities to provide choices for electricity customers to purchase power from environmentally preferred sources. Customers thereby agree to pay higher tariffs for “Green Electricity” and the utilities guarantee to produce the corresponding amount of electricity by using “Green Energy Sources”, e.g. wind energy.

3.1.3. *South and Central America*

Despite large wind energy resources in many regions of South and Central America, the development of wind energy is very slow. This is due to the lack of a sufficient wind energy policy as well as to low electricity prices. Many wind projects in South America have been financially supported by international aid programs. Argentina, however, has introduced a new policy at the end of 1998, which offers financial support to wind energy generation. In Brazil, some regional governments and utilities have started to offer higher feed-in tariffs for wind power [110]. The typical size of existing wind turbines is around 300 kW. Larger wind turbines are difficult to install, due to infrastructural limitations for larger equipment, e.g. cranes.

Offshore wind projects are not planned, but further small to medium-size (≤ 30 MW) projects are under development onshore (see Table 10).

3.1.4. Asia and the Pacific

India achieved an impressive growth in wind turbine installation in the middle of the 90s, the “Indian Boom”. In 1992/93, the Indian government started to offer special incentives for renewable energy investments, e.g. a minimum purchase rate was guaranteed as well as a 100% tax depreciation was allowed in the first year of the project. Furthermore, a “power banking” system was introduced, which allows electricity producers to “bank” their power with the utility and avoid being cut off during times of load shedding. Power can be banked for up to one year. In addition, some Indian States have introduced further incentives, e.g. investment subsidies. This policy led to a fast development of new installations between 1993 and 1997. Then the development slowed down, due to uncertainties regarding the future of the incentives (various editions of [8]).

The wind energy development in China is predominately driven by international aid programs, despite some government programs to promote wind energy, e.g. the “Ride-the-Wind” program of the State Planning Commission. Between 1999 and 2004, the World Bank plans to support 5 wind projects with a total installed capacity of 190 MW [110].

In Japan, demonstration projects testing different wind turbine technologies dominated the development. At the end of the 90s, the first commercial wind energy projects started operation on the islands of Hokkaido and Okinawa. The interest in wind power is constantly growing in Japan.

Also at the end of the 90s, the first wind energy projects materialised in New Zealand and Australia. The main drivers for wind energy development in Australia are green pricing programs.

In China and India, the typical wind turbine size is around 300 kW, however, some 500/600 kW wind turbines have also been installed. In Australia, Japan and New Zealand, the 500 to 600 range is predominant, however, first projects in Japan and Australia also use 1.5 MW turbines (see Table 11).

Table 10
Operational Wind Power Capacity in South and Central America^a

Country	Installed capacity [MW]	
	End 1995	End 2001
Costa Rica	0	51
Argentina	3	14
Brazil	2	20
Caribbean	4	13
Mexico	2	5
Total	11	103

^a Source: January edition 1997 and 2002 of [8].

Table 11
Operational wind power capacity in Asia and the Pacific^a

Country	Installed capacity [MW]	
	End 1995	End 2001
India	565	1,426
China	44	361
Sri Lanka	0	3
South Korea	0	8
Taiwan	0	3
Japan	5	250
New Zealand	2	37
Australia	10	74
Total	625	2,162

^a Source: January edition 1997 and 2002 of [8].

3.1.5. The Middle East and Africa

The wind energy development in Africa is very slow. Most projects require financial support by international aid organisations, as only limited regional support exists. Projects are planned in Egypt, where the government agency for New and Renewable Energy Authority (NREA) would like to build a 600 MW project near the city of Zafarana. Further projects are planned in Morocco (250 MW) as well as in Jordan (25 MW) ([110] and various editions of [8]; see Table 12).

The typical wind turbine size used in this region is around 300 kW, but plans exist to use 500/600 kW in future projects.

3.2. Overview of stand-alone generation

Stand-alone systems are usually used to power remote houses or remote technical applications, for example for telecommunication systems. The wind turbines used

Table 12
Operational wind power capacity in the Middle East and Africa^a

Country, region	Installed capacity [MW]	
	End 1995	End 2001
Iran	1	11
Israel	6	8
Egypt	5	125
Morocco	0	54
Jordan	1	2
Rest of Africa	0	3
Total	12	203

^a Source: January edition 1997 and 2002 of [8].

for these applications can vary between a few watts and 50 kW. For village or rural electrification systems up to 300 kW, wind turbines are utilised in combination with a diesel generator and sometimes a battery system.

Stand-alone wind turbine systems are also used world-wide to provide mechanical power for pumping drinking and irrigation water or for pumping oil.

Details regarding the world-wide installed capacity of small-scale or stand-alone wind turbines are not available. Also regional data are limited. China, for example, claims to have installed more than 110,000 small turbines (50 to 200 W). These turbines are mainly used to provide power to nomadic herdsman or farms [33].

Experts predict that the demand for stand-alone systems will grow significantly in the near future. This growth will be driven by the set-up of rural electrification programs in many parts of the world. In Brazil, Mexico, Indonesia, Philippines and South Africa such programs are supported by local utilities. In Indonesia, China, Russia, Mexico, Mauritania and Argentina, similar programs are supported by international aid programs and the World Bank is financing a program in Brazil [129, 32, 35 36].

3.3. Wind energy potential

Often wind energy is discussed in the context of the theoretically available potential. Wind energy potential studies show that the world-wide wind resources are abundant [187, 38, 101]. Matthies and Garrad, [144], for example, found that useful offshore potential in European waters alone account for around 2,500 TWh/year ([100]). This is about 85% of the electricity consumption in Europe in 1997 (see also [127]).

The results of wind energy resource studies depend on the quality of the available wind energy data as well as on the assumptions about technology and available space. Therefore, such studies can only provide an approximation of the overall wind energy potential. Furthermore, it is important to consider that the wind energy potential can vary significantly for different regions (see also 13.2).

4. The basics

The source of wind energy as well as the physical limitations in harvesting this natural resource is discussed next. In addition, a brief overview of the different wind turbine design principles is given.

4.1. The wind

Air masses move because of different thermal conditions of the masses. This motion of the air masses can be found as a global phenomenon, i.e. jet stream, as well as a regional phenomenon. The regional phenomenon is determined by orographic conditions, e.g. the surface structure of the area as well as by global phenomena.

Wind turbines utilise the wind energy near the ground. The wind conditions in

this area, known as the boundary layer, are influenced by the energy transferred from the undisturbed high-energy stream of the geostrophic wind to the layers below as well as by regional conditions. Due to the roughness of the ground, the wind stream near the ground is turbulent.

The wind speed changes with height and the wind speed share depends on the local conditions. There is also a wind direction share over height. Wind turbines therefore experience a wind speed share as well as wind direction share across the rotor, which result in different loads across the rotor.

As most wind energy textbooks describe the known knowledge regarding the wind speed share and wind direction share within the atmospheric boundary layer in more detail, see e.g. [29, 30, 31, 67], no further details will be given. For a detailed discussion of wind power meteorology, see [158, 157, 131]. It is, however, important to mention that most textbooks only cover the behaviour of the wind over flat, uniform terrain. The analysis of the wind share over complex terrain is discussed in more detail for example in [139, 48, 155].

Another important issue is the long-term variations of the wind resources. Different studies regarding this issue have been conducted (see [158], p. 33; [62, 177]). Based on these studies, Petersen et al. estimate that the variation of the mean power output from one 20-year period to the next has a standard deviation of 10% or less. Hence, the uncertainty of the wind resource is not large over the lifetime of a wind turbine, which is an important factor for an economic evaluation of a wind turbine. In many locations in the world, hydropower generation faces a higher uncertainty regarding the availability of water, than wind power [47].

4.2. The physics

The power of the wind that flows at speed V through an area A is ρAV , therefore

$$\text{Power of wind} = \frac{1}{2} \rho AV^3 \text{ [watt]}$$

where ρ =air density (kg/m³) and V =wind speed (m/s).

The power in the wind is proportional to the air density ρ , the intercepting area A and the velocity V to the third power. The air density is a function of air pressure and air temperature, which both are functions of the height above sea level:

$$\rho(z) = P_0 / (R \cdot T) \exp(-g \cdot z / (R \cdot T))$$

where $\rho(z)$ =air density as a function of altitude (kg/m³); P_0 =standard sea level atmospheric pressure (kg/m³); R =specific gas constant for air (J/K mol); T =temperature (K); g =gravity constant (m/s²); z =altitude above sea level (m).

The power in the wind is the total available energy per unit of time. The power in the wind is converted into the mechanical-rotational-energy of the wind turbine rotor, which results in a reduced speed of the air mass. The power in the wind cannot be extracted completely by a wind turbine, as the air mass would be stopped completely in the intercepting rotor area. This would cause a “congestion” of the cross-sectional area for the following air masses.

The theoretical optimum for utilising the power in the wind by reducing its velocity was first discovered by Betz, in 1926 [25]. According to Betz, the theoretically maximum power that can be extracted from the wind is

$$P_{\text{Betz}} = \frac{1}{2} \cdot \rho \cdot A \cdot v^3 \cdot C_{P_{\text{Betz}}} = \frac{1}{2} \cdot \rho \cdot A \cdot v^3 \cdot 0.59$$

Hence, even if a power extraction without any losses would be possible, only 59 percent of the wind power could be utilised by a wind turbine. For further details, see wind energy textbooks, e.g. [67, 30, 31].

Many textbooks, however, do not mention that Betz did not consider the impact of unavoidable swirl losses. For turbines with a high tip speed ratio, $X > 3$, and an optimum blade geometry, these losses are very low. The tip speed ratio, X , of a rotor is defined as:

$$X = V_{\text{tip}} / V_{\text{wind}} = \omega R / V_0$$

For turbines with a low tip speed ratio, e.g. the American farm windmill with $X \approx 1$, the swirl losses reduce the maximum power coefficient, $C_{P, \text{max}}$, to ≈ 0.42 [30, 31].

4.3. Types of wind turbines

Wind energy conversion systems can be divided into those which depend on aerodynamic drag and those which depend on aerodynamic lift. The early Persian (or Chinese) vertical axis windwheels utilised the drag principle. Drag devices, however, have a very low power coefficient, with a $C_{P, \text{max}}$ of around ≈ 0.16 [30, 31].

Modern wind turbines are predominately based on the aerodynamic lift. Lift devices use airfoils (blades) that interact with the incoming wind. The force resulting from the airfoils body intercepting the air flow does not consist only of a drag force component in the direction of the flow but also of a force component that is perpendicular to the drag: the lift forces. The lift force is a multiple of the drag force and therefore the relevant driving power of the rotor. By definition, it is perpendicular to the direction of the air flow that is intercepted by the rotor blade, and via the leverage of the rotor, it causes the necessary driving torque [174, 30, 31, 67, 33].

Wind turbines using the aerodynamic lift can be further divided according to the orientation of the spin axis into horizontal-axis and vertical-axis type turbines. Vertical-axis turbines, also known as Darrieus after the French engineer who invented it in the 1920s, use vertical, often slightly curved symmetrical airfoils. Darrieus turbines have the advantage that they operate independently of the wind direction and that the gearbox and generating machinery can be placed at ground level. High torque fluctuations with each revolution, no self-starting capability as well as limited options for speed regulations in high winds are, however, major disadvantages. Vertical-axis turbines were developed and commercially produced in the 70s until the end of the 80s. The largest vertical-axis wind turbine was installed in Canada, the ECOLE C with 4200 kW. Since the end of the 80s, however, the research and development of vertical-axis wind turbines has almost stopped world-wide [30, 31, 67, 33].

The horizontal-axis, or propeller-type, approach currently dominates the wind tur-

bine applications. A horizontal-axis wind turbine consists of a tower and a nacelle that is mounted on the top of a tower. The nacelle contains the generator, gearbox and the rotor. Different mechanisms exist to point the nacelle towards the wind direction or to move the nacelle out of the wind in the case of high wind speeds. On small turbines, the rotor and the nacelle are oriented into the wind with a tail vane. On large turbines, the nacelle with rotor is electrically yawed into or out of the wind, in response to a signal from a wind vane.

Horizontal-axis wind turbines typically use a different number of blades, depending on the purpose of the wind turbine. Two or three bladed turbines are usually used for electricity power generation. Turbines with twenty or more blades are used for mechanical water pumping.

The number of rotor blades is indirectly linked to the tip speed ratio, see Fig. 1. Wind turbines with a high number of blades have a low tip speed ratio but a high starting torque. This high starting torque can be utilised for fully automatically starting water pumping when the wind speed increases. A typical example for such an application is the American farm windmill. Wind turbines with only two or three blades have a high tip speed ratio, but only a low starting torque. These turbines might need to be started, if the wind speed reaches the operation range. But a high tip speed ratio allows the use of a smaller and therefore lighter gearbox to achieve the required high speed at the driving shaft of the power generator [183, 30, 31, 67, 33].

Apart from the above discussed wind turbine design philosophies, inventors frequently come up with new designs, using some kind of power argumentation, for instance. None of these inventions have given sufficient large-scale performances yet. For the current status of power argumentation wind turbines, see [185, 108].

5. Technology

The following chapter will provide a more in-depth overview of the technology trends of horizontal-axis, medium to large size grid-connected wind turbines (≥ 100 kW). This type of wind turbine currently has the largest market share and it is expected also to dominate the development in the near future.

5.1. Design approaches

Horizontal-axis wind turbines can be designed in different ways. Thresher (et al.) [183] distinguish three design philosophies, see Table 13. Modern grid-connected wind turbines usually follow the “C” approach, as it results in

- better power quality;
- lower tip-speed ratios than approach “B”, hence lower visual disturbances;
- lower material requirements than in approach “A”, as the structure does not need to withstand high wind loads, hence lower cost.

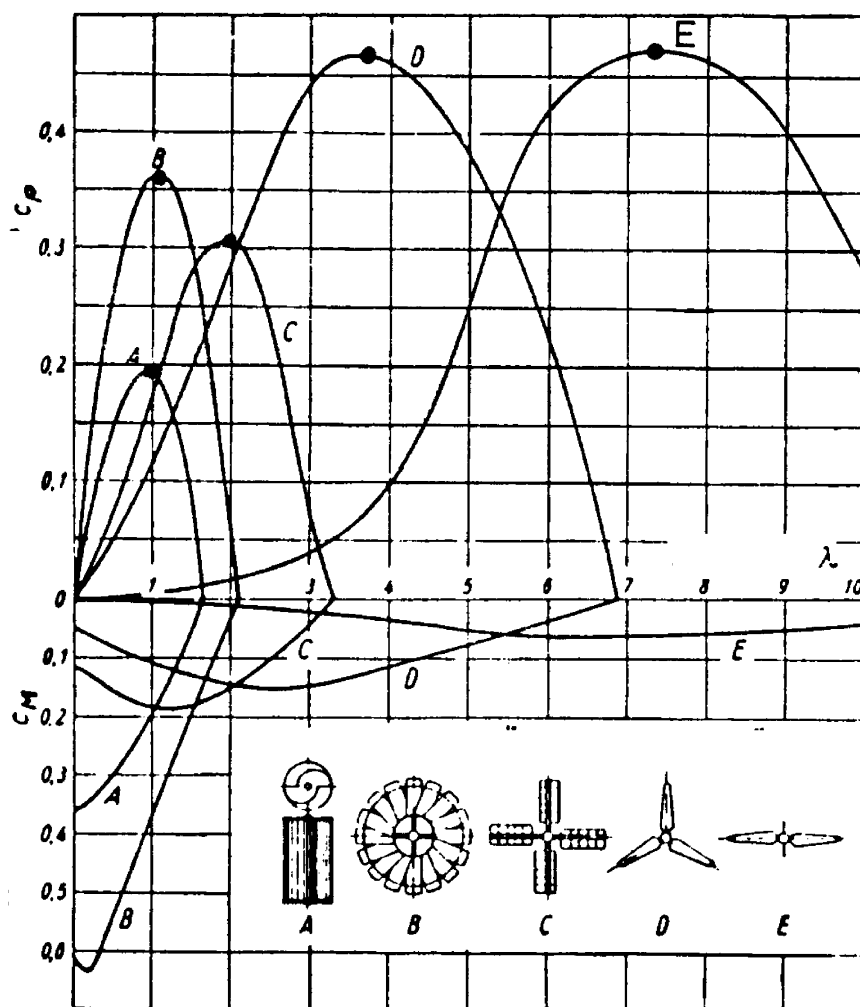


Fig. 1. Power coefficient (C_p) and torque (C_M) of windwheels varying in construction versus tip speed (λ); A, B, C=typical windwheels with a low tip speed ratio; D, E=typical windwheels with a high tip speed ratio (source: [30], page 163).

Different companies also investigate combinations of the different approaches. However, the “C” approach currently dominates the commercial market. See [183] for more details.

Each of the design approaches leaves a high degree of freedom regarding certain design details. For example, depending on the wind environment, different aerodynamic rotor diameters can be utilised. On high-wind speed sites, usually smaller rotor diameters are used with an aerodynamic profile that will reach the maximum efficiency between 14–16 m/s. For low-wind sites, larger rotors will be used but with an aerodynamic profile that will reach the maximum efficiency already between

Table 13
Basic design approaches^a

A	<p>Turbines designed to withstand high wind loads</p> <ul style="list-style-type: none"> ● Optimise for reliability ● High solidity but non-optimum blade pitch ● Three or more blades ● Lower rotor tip speed ratio <p>Precursor: Gedser mill</p>
B	<p>Turbines designed to be compliant and shed loads</p> <ul style="list-style-type: none"> ● Optimise for performance ● Low solidity, optimum blade pitch ● One or two blades ● Higher rotor tip speed ratio <p>Example: Hütter turbine</p>
C	<p>Turbines designed to manage loads mechanically and/or electrically</p> <ul style="list-style-type: none"> ● Optimise for control ● Mechanical and electrical innovations (flapping or hinged blades, variable speed generators, etc.) ● Two or three blades ● Moderate rotor tip speed ratio <p>Example: Smith–Putnam</p>

^a Source: Thresher et al. [183].

12–14 m/s. In both cases, the aim is to maximise the yearly energy harvest. In addition, wind turbine manufactures have to consider the overall cost, including the maintenance cost over the lifetime of the wind turbine.

The most important design variables are discussed next, e.g. number of blades, power control system and generation/transmission system. For further details regarding the design of wind turbines, see [160, 183, 30, 31, 44, 45, 33, 23, 43, 41, 26, 29, 42, 54, 63] and [55] pp. 26–47 for an overview of related articles.

5.2. Two or three-bladed wind turbines

Currently, three-bladed wind turbines dominate the market for grid-connected, horizontal-axis wind turbines. Two-bladed wind turbines, however, have the advantage that the tower top weight is lighter and, therefore, the whole supporting structure can be built lighter, and therefore very likely incur lower costs.

Three-bladed wind turbines have the advantage that the rotor moment of inertia is easier to understand and, therefore, often better to handle than the rotor moment of inertia of a two-bladed turbine [183]. Furthermore, three-bladed wind turbines are often attributed “better” visual aesthetics and a lower noise level than two-bladed wind turbines. Both aspects are important considerations for wind turbine utilisation in highly populated areas, e.g. the European coastal areas.

5.3. Power control

Wind turbines reach the highest efficiency at the designed wind speed, which is usually between 12 to 16 m/s. At this wind speed, the power output reaches the rated capacity. Above this wind speed, the power output of the rotor must be limited to keep the power output close to the rated capacity and thereby reduce the driving forces on the individual rotor blade as well as the load on the whole wind turbine structure. Three options for the power output control are currently used:

5.3.1. Stall regulation

This principle requires a *constant* rotational speed, i.e. independent of the wind speed. A constant rotational speed can be achieved with a grid-connected induction generator. Due to the airfoil profile, the air stream conditions at the rotor blade change in a way that the air stream creates turbulence in high wind speed conditions, on the side of the rotor blade that is not facing the wind. This effect is known as stall effect, see also Fig. 2.

The effect results in a reduction of the aerodynamic forces and, subsequently, of the power output of the rotor. The stall effect is a complicated dynamic process. It is difficult to calculate the stall effect exactly for unsteady wind conditions. Therefore, the stall effect was for a long time considered to be difficult to use for large wind turbines. However, due to the experience with smaller and medium-sized turbines, blade designers have learned to calculate the stall phenomenon more reliably. Today, even some manufacturers of megawatt turbines use stall-regulation, but the first prototypes of multi-megawatt wind turbines still avoid stall regulation (see overview of wind turbines in Section 5.7).

Figure 3 shows a typical power output chart of a turbine using stall control.

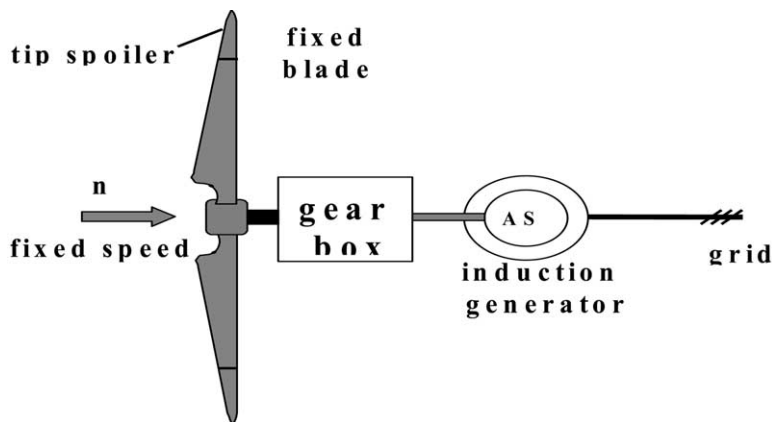


Fig. 2. Danish type of wind turbine with induction generator (constant rotational speed).

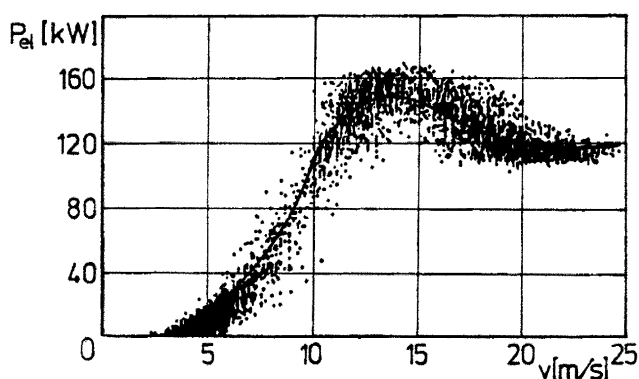


Fig. 3. Typical power output chart of a turbine using stall control (BONUS 150 kW, $D=23$ m, 10 min means are shown. Source: [30], p. 75.

5.3.2. Pitch regulation

By pitching the rotor blades around their longitudinal axis, the relative wind conditions and, subsequently, the aerodynamic forces are affected in a way so that the power output of the rotor remains constant after rated power is reached. The pitching system in medium and large grid-connected wind turbines is usually based on a hydraulic system, controlled by a computer system. Some manufacturers also use electronically controlled electric motors for pitching the blades. This control system must be able to adjust the pitch of the blades by a fraction of a degree at a time, corresponding to a change in the wind speed, in order to maintain a constant power output.

The thrust of the rotor on the tower and foundation is substantially lower for pitch-controlled turbines than for stall-regulated turbines. In principle, this allows for a reduction of material and weight, in the primary structure. Pitch-controlled turbines achieve a better yield at low-wind sites than stall-controlled turbines, as the rotor blades can be constantly kept at optimum angle even at low wind speeds.

Stall-controlled turbines have to be shut down once a certain wind speed is reached, whereas pitch-controlled turbines can gradually change to a spinning mode as the rotor operates in a no-load mode, i.e. it idles, at the maximum pitch angle. An advantage of stall-regulated turbines consists in that in high winds—when the stall effect becomes effective—the wind oscillations are converted into power oscillations that are smaller than those of pitch-controlled turbines in a corresponding regulated mode. Particularly, fixed-speed pitch-controlled turbines with a grid-connected induction generator have to react very quickly to gusty winds. This is only possible within certain limits, otherwise huge inertia loads counteracting the pitching movement will be caused. Figure 5 shows the output characteristics typical of a wind turbine using pitch control.

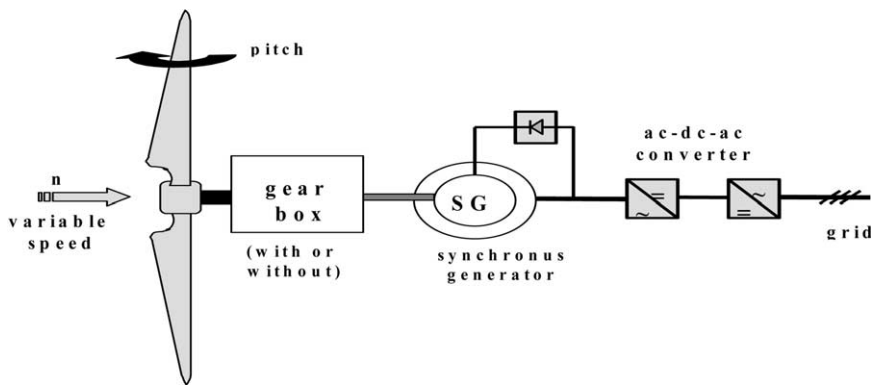


Fig. 4. Pitch-controlled variable speed wind turbine with synchronous generator and ac–dc–ac power conversion.

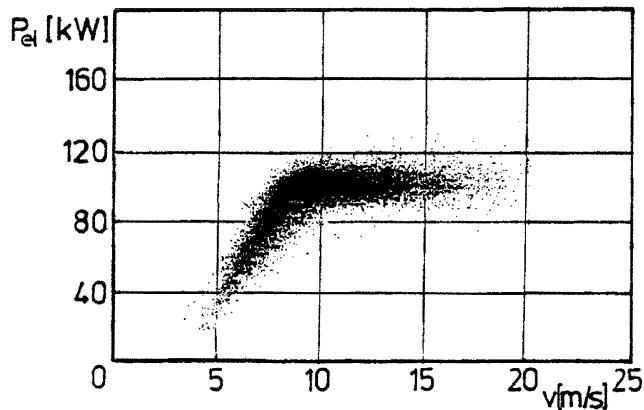


Fig. 5. Output characteristics typical of a wind turbine using pitch control (DEBRA 100 kW, $D=25$ m, [21], 1 s mean values are shown). Source: [30], p. 76.

5.3.3. Active stall regulation

This regulation approach is a combination between pitch and stall. At low wind speeds, blades are pitched like in a pitch-controlled wind turbine, in order to achieve a higher efficiency and to guarantee a reasonably large torque to achieve a turning force. When the wind turbine reaches the rated capacity, the active stall-regulated turbine will pitch its blades in the opposite direction than a pitch-controlled machine does. This movement will increase the angle of attack of the rotor blades in order to make the blades go into a deeper stall. It is argued that active stall achieves a smoother limiting of power output, similar to that of pitch-controlled turbines without their ‘nervous’ regulating characteristics. It preserves, however, the advantage of pitch-controlled turbines to turn the blade into the low-load ‘feathering position’, hence thrust on the turbine structure is lower than on a stall-regulated turbine.

Other control methods are ailerons used to yaw the rotor partly out of the wind

in order to decrease power. Ailerons are flaps in the blades, just like the flaps in aircraft wings, however, they are not used by the wind energy industry. Yawing is only used for small wind turbines (~5 kW or less), as the stress on the entire structure is very difficult to handle with larger wind turbines.

If the wind speed reaches the cut-out wind speed (usually between 20 and 30 m/s), the wind turbine shuts off and the entire rotor is turned out of the wind to protect the overall turbine structure. Because of this procedure, possible energy that could have been harvested will be lost. However, the total value of the lost energy over the lifetime of the wind turbine will usually be smaller than the investments that will be avoided by limiting the strength of the turbine to the cut-out speed.

Limiting the strength of the turbine requires emergency or overspeed control systems to protect the wind turbine in case of a failure of the brakes. Typical overspeed control systems are tip brakes or pitchable tips included in the rotor blades [33].

For high wind speed sites, the cut-out wind speed and the setpoint for starting up the wind turbine again after the wind turbine was stopped and turned out of the wind, can have a significant impact on the energy yield. Typically, a wind turbine shuts down every time the 10 minute wind speed average is above the cut-out wind speed, e.g. 25 m/s. The setpoint for starting up the wind turbine varies widely throughout the industry. Often, wind turbines start up operation when the 10 minute average wind speed drops below 20 m/s. However, the setpoint can vary between 14 and 24 m/s, depending on the wind turbine type. Low setpoints for resuming the wind power production have a negative impact on the energy production. The above phenomenon is described in specialist publications as the hysteresis effect or hysteresis loop [186].

Details of the rotor aerodynamics are not covered in this paper, as a review of the current status of rotor aerodynamics is available in [174] as well as in [40]. It is, however, important to mention that most modern rotor blades of large wind turbines are made of glass fibre reinforced plastics, (GRP), i.e. glass fibre reinforced polyester or epoxy, and are equipped with a lightning protection system.

5.4. Transmission and generator

The power generated by the rotor blades is transmitted to the generator by a transmission system. The transmission system consists of the rotor shaft with bearings, brake(s), an optional gearbox, as well as a generator and optional clutches. In real life, there is a large variety regarding the placement of these components, see Figs 2 and 4 and [30, 31] for a detailed discussion of the placement.

Most wind turbine manufacturers use six-pole induction (asynchronous) generators, others use directly driven synchronous generators. In the power industry, in general, induction generators are not very common for power production, but induction motors are used world-wide. The power generation industry uses almost exclusively large synchronous generators, as these generators have the advantage of a variable reactive power production, i.e. voltage control.

5.4.1. Synchronous generators

Synchronous generators with 500 kW to 2 MW are significantly more expensive than induction generators with a similar size. In addition, direct grid-connected synchronous generators have the disadvantage that the rotational speed is fixed by the grid frequency and the number of pairs of poles of the generator. Hence, fluctuations in the rotor power output, e.g. due to gusts, lead to a high torque on the drivetrain as well as high power output fluctuations, if other means, e.g. softer towers, are not used to reduce the impact of gusts. Therefore, directly grid-connected synchronous generators are usually not used for grid-connected wind turbines. They are applied in stand-alone systems sometimes, where the synchronous generator can be used for reactive power control in the isolated network.

An option for the utilisation of synchronous generators for wind turbines is the decoupling of the electric connection between the generator and the grid through an intermediate circuit. This intermediate circuit is connected to a three-phase inverter that feeds the grid with its given voltage and frequency. Today, pulse-width modulated (PWM) inverters are commonly used. For further discussions of details regarding the coupling of variable speed generators to the network, see [44, 45]).

The decoupling of grid and the rotor/generator allows a variable speed operation of the rotor/generator system. Fluctuations in the rotor output lead to a speed-up or slow-down of the rotor/generator. This results in a lower torque on the drivetrain as well as a reduction of power output fluctuations. Furthermore, it is important to remember that the maximum power coefficient occurs only at a single tip speed ratio. Hence, with a fixed-speed operation the maximum power coefficient is only reached at one wind speed. With a variable speed operation, the rotor speed can accelerate and decelerate in accordance with the variations in the wind speed in order to maintain the single tip speed ratio that leads to a maximum power coefficient [183].

The industry uses direct-driven variable speed synchronous generators with large-diameter synchronous ring generators (see Fig. 4). The variable, direct-driven approach avoids the installation of a gearbox, which is essential for medium and large-scale wind turbines using an induction generator. The gearbox is required to increase the rotational speed from around 20 to 50 revolutions per minute (rpm) on the rotor side to, for example, 1200 rpm (for 50 Hz) on the induction generator side. This rotational speed on the induction generator side is necessary to produce power at the required network frequency of 50 Hz (or 60 Hz). The required rpm for the generator depends on the number of pole pairs.

The direct-driven synchronous ring generator of the Enercon E40 (500 kW), on the other hand, operates with a variable rotational speed of 18 to 41 rpm.

5.4.2. Induction generators

Induction generators have a slightly softer connection to the network frequency than synchronous generators, due to a changing slip speed. This softer connection slightly reduces the torque between rotor and generator during gusts. However, this almost fixed-speed operation still leads to the problem that overall efficiency during low wind speeds is very low. The traditional Danish approach to overcoming this

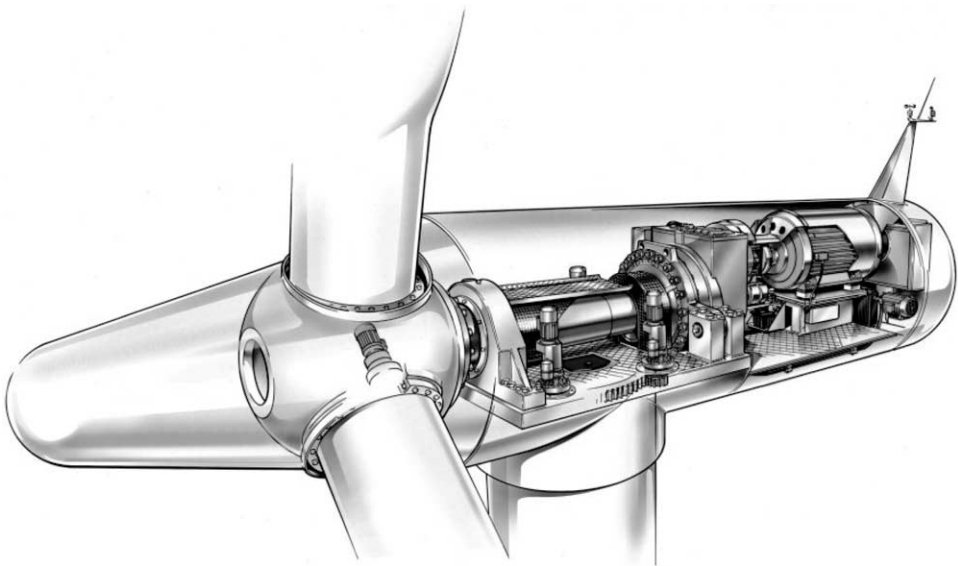


Fig. 6. Nacelle BONUS 1 MW. Courtesy of BONUS Energy A/S, Denmark.

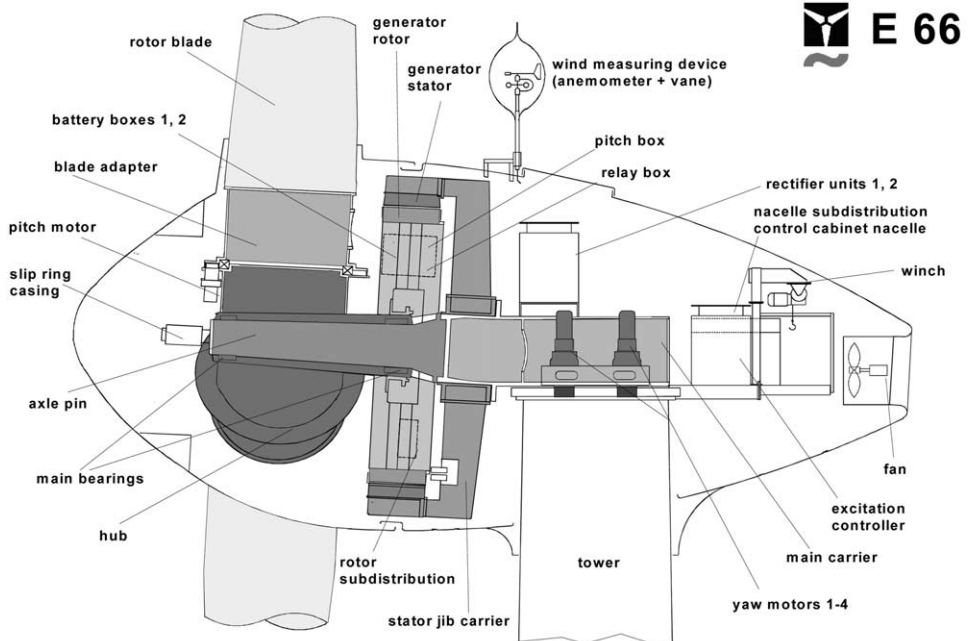


Fig. 7. Nacelle Enercon 1.5 MW. Courtesy of Enercon, Germany.

Table 14

Size and weight data for representative turbines^a

Type	Control system, (P) pitch, (S) stall, (AS) active stall	Rotor diameter (m)	Number of blades	Rated capacity (kW)	Nacelle and rotor weight (kg)	Weight per swept area (kg/m ²)	Generator
Bonus 300 kW	S	31	3	300	14500	19.2	AG
Bonus 1 MW	AS	54	3	1000	63000	27.5	AG
Bonus 1.3 MW	AS	62	3	1300	80900	26.9	AG
Bonus 2 MW	AS	76	3	2000	125000	27.7	AG
Carter	AS	24	2 (T)	300	4431	10	AG
DeWind D4	P	46	3	600	–	–	DFAG
DeWind D6	P	62	3	1000	–	–	DFAG
DeWind D8	P	80	3	2000	–	–	DFAG
Enercon E-30	P	30	3	230/ 280	14650	20.7	DD
Enercon E-40	P	40.3	3	500	29500	23.1	DD
Enercon E-58	P	58	3	1000	92000	34.1	DD
Enercon E-66/1.5	P	66	3	1500	99590	29.1	DD
Enercon E-66/1.8	P	70	3	1800	101100	26.2	DD
Enron 900	P	55	3	900	–	–	DFAG
Enron TW 1.5	P	65	3	1500	74000	22.3	DFAG
Enron TW 2.0	P	70.5	3	2000	80000	20.5	DFAG
Fuhrländer:							
FL30	S	13	3	30	1360	10.2	AG
FL100	S	21	3	100	9000	26.0	AG
FL250	S	29.5	3	250	14700	20.8	AG
FL800	S	50	3	800	55000	30.4	AG
FL1000	S	54	3	1000	59000	25.7	AG
FL MD 70	P	70	3	1500	84200	21.8	DFAG
FL MD 77	P	77	3	1500	87500	18.8	DFAG
Gamesa G52	P	52	3	850	37500	17.6	DFAG
Jeumont J48	P	48	3	750	–	–	DD+PM
Lagerwey 18/ 80	P	18	2 flex	80	3000	11.8	AG
Lagerwey 27/ 250	P	27	2 flex	250	10000	17.5	AG
Lagerwey 50/ 750	P	50.5	3	750	–	–	DD+PM
Made AE-52	P	52	3	800	37000	17.4	DVAG
Made AE-66	S	66	3	1300	72000	24.6	AS
NEG Micon:							
NM 600/ 43	S	43	3	600	35000	24.1	AG
NM 750/ 48	S	48	3	750	–	–	AG
NM 1000/ 60	S	60	3	1000	–	–	AG
NM 1500/ 64	AS	64	3	1500	–	–	AG
NM 2000/ 72	AS	72	3	2000	–	–	AG
NM 2500/ 80	P	80	3	2500	–	–	DFAG
Nordic 1000	S	54	2	1000	45000	19.6	VAG
Nordex N-29	S	29.7	3	250	16800	24.2	AG
Nordex N-43	S	43	3	600	35500	24.5	AG
Nordex N-54	S	54	3	1000	69800	30.5	AG

(continued on next page)

Table 14 (continued)

Type	Control system, (P) pitch, (S) stall, (AS) active stall	Rotor diameter (m)	Number of blades	Rated capacity (kW)	Nacelle and rotor weight (kg)	Weight per swept area (kg/m ²)	Generator
Nordex N-63	S	63	3	1300	69400	24.5	AG
Nordex N-80	P	80	3	2500	119300	23.7	DFAG
Riva Calzaoni M30-52	P	33	1	–	13500	15.8	AG
RePower 48/600	S	48	3	600	–	–	AG
RePower 48/750	S	48	3	750	–	–	AG
RePower 1000/57	P	57	3	1000	–	–	AG
Südwind S33	S	33.4	3	350	–	–	AG
Südwind S46/ 750	P	46	3	750	–	–	DFAG
Tacke TW 600	S	43	3	600	33000	22.7	AG
Turbowind T400	AS	34	3	400	–	–	AG
Turbowind T600	AS	48	3	600	–	–	AG
Vestas:							
V29- Optislip	P	29	3	225	13000	19.7	VAG
V44- Optislip	P	44	3	600	25700	16.9	VAG
V63- Optislip	P	63.6	3	1500	74000	23.7	VAG
V66- Optislip	P	66	3	1650	78000	22.8	VAG
V80- Optislip	P	80	3	2000	95000	18.9	VAG
V52-Optispeed	P	52	3	850	32000	15.0	DFAG
V66-Optispeed	P	66	3	1750	80000	23.4	DFAG
V80-Optispeed	P	80	3	2000	95000	18.9	DFAG
Vergnet 15/60	P+S	15	2	60	2400	–	AG
Vergnet 26/220	P	26	2	220	5400	–	AG
WinWind WWD-1	P	56	3	1000	64000	25.9	SG+PM
Zond 750	P	50	3	750	–	–	DFAG

^a DFAG=double fed asynchronous generator; DD=Direct driven, variable speed, electrically excited synchronous generator; VAG=asynchronous generator with variable slip; AG=asynchronous generator; SG=synchronous generator; PM=permanent magnets. Source: [183], [150], and authors.

problem is to use two induction generators, one small and one large. Today, the same effect is achieved with pole changing machines. With this approach, two rotational speeds are possible. The small induction machine is connected to the grid during low wind speeds. When the wind speed increases, the small generator is switched off and the large generator is switched on. The operating point of the larger generator lies at a higher rotational speed.

To further reduce the load on the wind turbine and to make use of the advantages of variable-speed generation with induction generators, it is reasonable to further decouple rotor speed and grid frequency. There are various approaches to achieving a variable-speed operation within a certain operational range. Today, dynamic slip control, where the slip can vary between 1 and 10%, and double fed asynchronous

generators are most commonly used by the industry. For an overview of the different approaches, see [45], pp. 105.

The reactive power requirements are the disadvantage of induction generators. As a reactive power flow from the network is usually not desired by the network operators, turbines with induction generators are usually equipped with capacitors. These capacitors usually compensate the reactive power demand of the induction generators. Another setback of induction generators is the high current during the start-up of the generator, due to the required magnetising of the core. Controlling the voltage applied to the stator during the start-up and thereby limiting the current can solve the problem.

A description of synchronous and induction generators can be found in many standard textbooks. Heier [44, 45] provides a good overview regarding the different generator technologies currently used by the wind industry as well as future options for the design of wind turbine generators, e.g. permanently excited synchronous generators. Such generators have been tested in demonstration projects but are currently not applied in medium or large-scale wind turbines. They are, however, quite common in small-scale (10 kW or less) wind turbines.

The evaluation of the different wind turbine designs is difficult, even with production data, as the local wind resources can vary significantly between different locations. However, production data of existing wind turbines are an important source of information regarding wind turbine performance at particular locations. Wind turbine production data are often published by wind energy associations (see Section 11.1). Good resources regarding wind turbine performance data are also the following publications and research projects [9, 49, 13, 97].

5.5. Current trends and new concepts

Most wind turbine manufacturers are working on larger wind turbines in the multi-megawatt range, see Table 15. For those turbines, the so-called Danish Concept, based on fixed speed, stall regulation and asynchronous generator, is regarded as technically unfeasible.

The new concepts are based on variable speed operation with pitch control using either direct driven synchronous ring generator (Enercon/Lagerwey/Jeumont/Mtoores) or double fed asynchronous generators (Enron/Vestas/DeWind, etc.), see Tables 14 and 15.

Other companies (WinWind/Multibrid) are developing system designs that can be described as a combination of the two systems above. The design is a variable speed, pitch regulated wind turbine using a single stage gearbox, hence the high ratio gearing and generator speeds of 1500–1800 rpm of designs based on double fed asynchronous generators are avoided. The use of a single-stage gearbox allows the use of a slow rotating permanent magnet synchronous generator, which can be designed smaller and lighter than the large direct driven synchronous ring generators (see Figs 6 and 7).

In addition, the industry is working on an improvement of the efficiency on the electrical side of a wind power conversion system. Thus improvements include the

Table 15
Data of large wind turbines currently under development^a

Type	Country	Control system (P) pitch, (S) stall, (AS) active stall	Rotor diameter (m)	Number of blades	Rated capacity (kW)	(VS) variable speed (FS) fixed speed
NEG Micon:						
3000	DK+NL	P	90	3	3000	VS
DOWEC***	NL+DK	P	120	6	6000	VS
Wincon 2000	Denmark	AS	70	3	2000	FS
DeWind D9	Germany	P	90	3	3500	VS
Jeumont	France	P	-	3	1500	VS+PM
Enron 3.2	D+USA	P	104	3	3200	VS
Enron 3.6	D+USA	P	100	3	3600	VS
Lagerway/ ABB	NL+SE	P	72	3	2000	VS+PM*
Mitorres TWT 1500	Spain	P	72	3	1500	VS
Vestas V90	Denmark	P	90	3	3000	VS
Windformer/ABB	Sweden	P	90	3	3000	VS+PM**
Enercon E-112	Germany	P	112	3	4500	VS
RePower/N.O.K. 5	Germany	P	115	3	5000	VS
Pfleiderer/Multibrid	Germany	S+Tips (or P)	100	3	5000	VS

^a PM=permanent magnets; *=output voltage of 4000 V; **=output voltage of 25000 V; ***=Dutch wind energy converter; SE=Sweden; D=Germany; NL=The Netherlands; DK=Denmark. Source: author.

installation of permanent magnets in the generator (Jeumont/Lagerwey/WinWind/Windformer) or higher voltage output levels of the generator. Traditionally, wind turbine generators are operated at 690 V (Enercon 440 V), which require a transformer in the nacelle or at the bottom of the tower. Higher output voltages lead to a reduction of line losses and might make the installation of a transformer obsolete. Current research projects include the Lagerwey/ABB 2 MW project (output voltage 3000–4000 V) and the Windformer/ABB 3 MW turbine (output voltage 25000 V).

5.6. *Technology standards*

Wind energy standards become more and more important for ensuring a certain design quality of wind turbines or for defining performance testing, acoustic and meteorological measurements at a potential wind turbine site.

Many countries, e.g. Germany, Denmark, USA and India, have developed their own set of wind energy standards. However, the trend is to internationally harmonise the world-wide wind energy standards. More information about the international activities towards a standard can be obtained from the European Wind Turbine Standards (EWTS) Project [1] as well as from the American Wind Energy Association (AWEA), which is recognised by the American National Standards Institute (ANSI) as the only authorised wind energy standard-setting body in the United States [72].

The International Electrotechnical Commission (IEC) in Geneva, has defined and published international standards regarding wind energy technology, see for example [120]–[126], or see the IEC webpage [119] for further information.

5.7. *Wind turbine overview*

The following tables provide an overview of representative existing wind turbines as well as large wind turbines currently under development.

5.8. *Publications*

The following publications regularly contain papers and articles on the development of wind turbine technology:

Journal of Wind Engineering and Industrial Aerodynamics [4], Renewable Energy [5], Renewable Energy World [6], Wind Stats Newsletter [9], Wind Energy [10], Wind Energy Newsletter [11], Wind Engineering [12].

6. **Network integration**

In most parts of the world, wind energy supplies only a fraction of the total power demand. In other regions, for example in Northern Germany, Denmark or on the Swedish island of Gotland, wind energy supplies already a significant amount of the total energy demand. In 2000, wind energy supplied around 3.268 GWh out of 13,000

GWh (penetration of 25%) in the German province of Schleswig–Holstein. In Denmark, within the network area of Eltra (Jutland and Funen), wind power supplied 3,372 GWh out of 20,647 GWh (16.1%), see [154].

With increasing wind power penetration, the availability of wind power generation as well as its influence on the network becomes of particular interest (see also [18, 19, 28, 192]). The relevant issues are briefly discussed next.

6.1. Availability

Wind generation has a fluctuating power output, due to the variability of the wind speed. Table 16 lists causes and time scales of wind variations.

The fluctuations in the available wind energy caused by gusts result in power output fluctuations from the wind turbine. Such power fluctuations may affect the power quality of the network. A reduction of short-term power fluctuations can be achieved using variable-speed operated wind turbines as they are able to absorb short-term power variations by the immediate storage of energy in the rotating masses of the drive train, hence, a smoother power output is achieved than with strongly grid-coupled turbines [141].

An additional smoothing effect is achieved when a wind farm consists of a large number of wind turbines, short-term fluctuations in the overall output are reduced due to the effect that gusts do not hit all wind turbines at the same time. Under ideal conditions, the variations of power output will drop with $1/\sqrt{n}$, where n is the number of wind generators [168]. For the time range of subseconds, Santjer et al. [168], however, found that the smoothing or compensating between different wind turbines in a wind farm cannot be expected, in general. Particularly during switching, e.g. the start-up of a wind farm, the grid interferences are higher than assumed by the $1/\sqrt{n}$ rule. Stampa [181] even found that wind turbines with direct grid-connected induction generators in a wind farm could fall into synchronism with their rotor azimuth position. This synchronism can cause high amplitudes in voltage fluctuations. Both situations can be avoided by co-ordinating the operation of the different wind turbines in a wind farm and by varying the electrical parameters of the wind farm grid.

Table 16
Causes and time scale of wind variation^a

Causes of variation	Time scale of variation
Gusts (turbulence)	Sub-second to second
Diurnal cycle	Daily
Inversion layers	Hours
Changing weather patterns	Hours to days
Seasonal cycle (monsoon)	Seasonal
Annual variation	Years

^a Source: Davitian [87].

The medium-term variations (hours) are also very important for network operation, as network operators have to dispatch other generation sources, if the wind energy power output varies strongly.

Figure 8 is based on the 1997 statistical analysis of 63 wind turbines (total 11.4 MW) installed in the area of Schleswig–Holstein. The figure shows the statistical average probability of a power output change of the total installed wind capacity from the mean power gradient of one hour (or four or twelve hours) to the next.

It can be seen that with a probability of 30 percent the hourly mean wind power output from one hour to the next will be $\pm 1\%$ of total installed capacity ($\pm 4\%$ from one four hourly mean to the next and $\pm 12\%$ between the twelve hourly means). The largest change in power output to be expected between hourly mean power output values is about 40% (probability 0.01 percent) of installed capacity (about 80% between 4 hourly means, and almost 100% between 12 hourly means). A Danish study [83] as well as a Dutch study, [39] p. 89, confirmed the relatively large compensation of the power variations between different wind turbines distributed over a large area. The Danish study, however, emphasised that the variations per minute can still be significant.

Long-term variations in wind speed, between one year and the next, are usually quite low, as discussed in Section 4.1.

6.2. Power quality

Wind turbines as well as all other equipment connected to the public grid affect the quality of the power in the grid. These effects include voltage fluctuations due to power fluctuations and may be flicker effects, voltage asymmetry and harmonics. Detailed discussion of these effects can be found in standard textbooks, e.g. [44, 45,

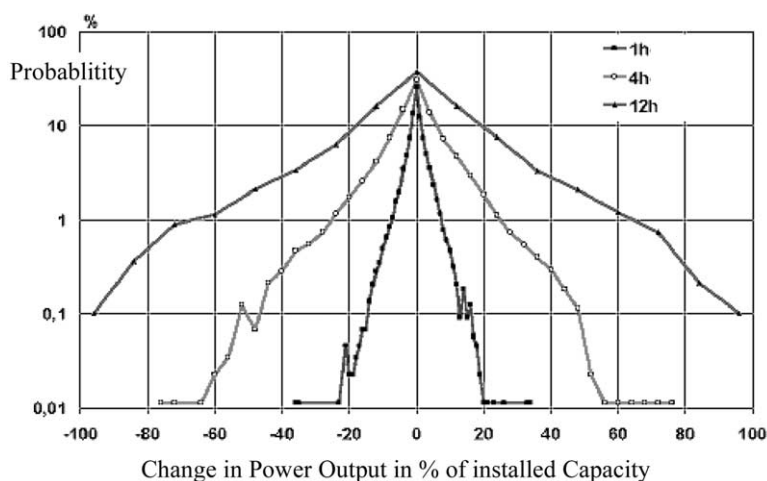


Fig. 8. Power gradients for extended periods (Schleswig–Holstein). Source: ISET [49], p. 50.

23]. To study the impact of wind turbines on the power network, detailed computer models of wind turbines are used, see e.g. [71].

The evaluation of the impact of wind turbines on the power quality is a complex problem, due to the unique design of each distribution network as well as the different types of wind turbines, e.g. variable speed or fixed speed, stall or pitch-regulated. Fixed-speed wind turbines, for example, produce a power pulsation emanating from the wind share over height, and the tower shadow effect. Such a power pulsation will cause voltage fluctuations on the grid, which in turn may cause flicker. Variable-speed as well as limited variable-speed turbines, e.g. with induction generators with variable slip, significantly reduce the power fluctuations due to wind share and tower shadow effect [142, 153].

The start-up of wind turbines is also an important issue. The grid connection during the start-up of stall-regulated fixed-speed wind turbines can cause high inrush currents, as the rotor torque cannot be exactly controlled to meet the required generator torque. Pitch-regulated fixed-speed as well as variable-speed wind turbines are able to achieve a smoother grid connection during start-up [153, 141, 142, 82].

Another issue is the introduction of harmonics and interharmonics. This issue is not relevant for fixed-speed but for variable-speed wind turbines, as they are equipped with a power converter that can emit harmonics or interharmonics during continuous operation. Line commutated inverters produce harmonics of low orders (250 to 350 Hz) and force commutated inverters using PWM and IGBT produce harmonics of high orders (≥ 6 kHz) [82]. Special filters are used to reduce harmonics. To limit the influence of harmonics on the grid power quality, power converters used within wind turbines should perform in accordance with international standards, e.g. IEC 61300-3 and 61000-4-7 [121, 120].

The steady-state voltage in a grid system also fluctuates, due to the fluctuations in load. This situation occurs particularly in weak grid systems, e.g. long, low-loaded, low-voltage transmission lines. The additional connection of wind farms may increase these voltage fluctuations, due to short as well as long-term fluctuations in the power output. However, wind turbines with a controllable power factor might also be able to reduce the voltage fluctuations if the power factor of the wind turbine is continuously adjusted according to the voltage fluctuations caused by the system load [170].

And finally, an increase of wind energy penetration might result in new phenomena, e.g. voltage collapse problems. As Denmark wants to increase its wind power penetration to 50% by the year 2030, detailed studies are currently conducted by Danish network operators, see e.g. [81]. One of the suggested solutions currently discussed is the installation of advanced HVDC technology within the distribution network or as transmission technology between the onshore network and large offshore wind farms, see [18, 94, 176].

A good source of further information in the area of network integration are the proceedings of the EWEA conference Wind Power for the 21st Century, which was held in Kassel, 25–27 September 2000. Other sources for information are [18, 19, 44, 45, 70, 78, 69, 18, 180, 95, 113, 154, 178, 192, 193, 196]. Also the regular wind

energy literature survey in wind energy (see Section 12.4) usually includes many references within the area of network integration and power quality.

7. Economics

In the 90s, the cost for manufacturing wind turbines declined by about 20% every time the number of manufactured wind turbines doubled [180]. Currently, the production of large-scale, grid-connected wind turbines doubles almost every three years. Similar cost reductions have been reported for PV solar and biomass, however, these technologies have slightly different doubling cycles. A similar cost reduction was achieved during the first years of oil exploitation about 100 years ago. But the cost reduction for electricity production between 1926 and 1970 in the USA, mainly due to economies of scale, was higher. An average cost reduction of 25% for every doubling of production is reported for this time period [171].

The Danish Energy Agency predicts that a further cost reduction of 50% can be achieved by 2020, and the EU Commission estimates in its White Book that energy costs from wind power will be reduced by at least 30% between 1998 and 2010 [180]. Other authors, though, emphasise that the potential for further cost reduction is not unlimited and very difficult to estimate [33].

A general comparison of the electricity production costs, however, is very difficult as production costs vary significantly between countries, due to the availability of resources, different tax structures or other reasons. In addition, market regulation can affect the electricity prices in different countries. The competitive bidding processes for renewable power generation in England and Wales (The Non-Fossil Fuel Obligation—NFFO), however, provides a good comparison of power production prices. Within this bidding process, potential project developers for renewable energy projects are invited to bid for building new projects. The developers bid under different technology brands, e.g. wind or solar, for a feed-in tariff or for an amount of financial incentives to be paid for each kWh fed into the grid by renewable energy systems. The best bidder(s) will be awarded their bid feed-in tariff for a predefined period.

Due to changes in regulations, only the price development of the last three bidding processes can be compared. They are summarised in Table 17. It shows that wind energy bidding prices decreased significantly, e.g. between the 1997 (NFFO4) and 1998 (NFFO5), the average decrease was 22%. Surprisingly, the average price of all renewables for NFFO5 is 2.71 British pence (p)/kWh, with some projects as low as 2.34 p/kWh, while the average Power Purchase Price (PPP) at the England and Wales spot market, based on coal, gas and nuclear power generation, was 2.455 p/kWh between April 1998 and April 1999.

The question emerges, why would a project developer accept a lower priced contract from NFFO, if he could also sell his energy for a higher price via the spot market? The reason probably is that NFFO is offering a 15-year fixed contract, hence the financial risk is reduced. Also, additional costs for trading via the spot market make the trade of a small amount of energy unfeasible. Furthermore, as project

Table 17

Successful bidding prices in British pence/kWh 1.99: 1 ECU=1 Euro=1.15 US\$=0.7 £^a

	NFFO3	NFFO4	NFFO5
Large wind	3.98–5.99	3.11–4.95	2.43–3.14
Small wind	–	–	3.40–4.60
Hydro	4.25–4.85	3.80–4.40	3.85–4.35
Landfill gas	3.29–4.00	2.80–3.20	2.59–2.85
Waste system	3.48–4.00	2.66–2.80	2.34–2.42
Biomass	4.90–5.62	5.49–5.79	–

^a Source: Office of Electricity Regulation [159].

developers have a period of five years to commission their plants, some developers have used cost prediction for their future projects based on large cost reductions during the following 5 years. For further discussion of wind power economics, see [107, 114, 115, 179].

8. Wind project issues

The future development of wind power world-wide will depend on the economics of wind power as well as on the public acceptance. The economics of wind power projects depend on the available wind speed, but investment failures can be caused by unreliable wind measurements or imprecise modelling of the wind flow. The public acceptance depends on the environmental impact of wind energy projects, e.g. its visual and noise impact or the impact on flora and fauna.

8.1. Wind measurement

The power in the wind is proportional to the third power of the wind speed, see Section 4.2. Hence, a 10% deviation of the expected wind speed corresponds to a 30% deviation in the expected power in the wind. Wind data for site evaluation therefore must be as accurate as possible and therefore wind speed measurements on site are necessary. Most wind energy textbooks, e.g. [30, 31, 32, 33], discuss the relevant issues in detail.

Wind measurements have the disadvantages that data are limited to one site and that it is often not possible to measure the wind speed and wind direction at the hub height of the wind turbine. Therefore, computer simulation tools have been developed to evaluate the wind conditions at hub height over a certain area by taking the wind data of a suitable reference point, e.g. from a wind measurement, and the local influences, e.g. obstacles, into consideration. The following publications provide an overview and discussion of the relevant aspects and the existing computer models: [158, 157, 48, 139, 85].

At least in Europe, the *Wind Atlas Analysis and Application Program*—WAsP,

developed by the Danish Risø National Laboratory, is the most commonly used computer tool in this field. In flat terrain, e.g. in Denmark and northern Germany, WAsP delivers reliable results. In complex, very rugged terrain, however, WAsP could lead to results outside an acceptable range, see [79, 163, 112, 116, 117].

As international wind energy developments in the last few years moved more and more into complex terrain, e.g. mountains, international research effort concentrated on analysing the error range of WasP as well as on improving the methodology, see [76, 156, 86]. In addition, new methodologies are under development leading to new computer simulation models, see [77, 99, 56, 145, 146, 147, 149, 152, 191]. Evaluation studies of the improved WAsP model and other, new computer simulation models are currently carried out.

8.2. *Environmental impact*

Wind energy can be regarded as environmentally friendly, however, it is not free of emissions. The production of the blades, the nacelle, the tower etc., the exploration of the material and the transport of equipment leads to the consumption of energy resources, hence emissions are produced as long as these energy resources are based on fossil fuel. These emissions are known as indirect emissions. Table 18 provides an overview of the most important emissions related to electricity production based on different power generation technologies. The data comprises direct emissions and indirect emissions. The calculation is based on the average German energy mix and on typical German technology efficiency.

In addition, the noise and the visual impact of wind turbines are important considerations for a public acceptance of wind energy technology, particularly if the wind turbines are located close to human settlements [66]. The noise impact can be reduced with technical means, e.g. variable speed or reduced rotational speed. The noise impact as well as the visual impact can also be reduced with appropriate siting of wind turbines in the landscape. Helpful guidelines as well as important examples for appropriate siting of wind turbines can be found in Stanton [64], Nielsen [56], Pasqualetti [58] as well as in Gipe [33].

9. **Special system applications**

Wind energy can be utilised for different purposes and in different climate zones. The following chapter presents the most interesting special applications for the use of wind energy.

9.1. *Cold weather*

Wind turbines installed in regions with extreme cold weather, e.g. in northern Scandinavia, Canada or in north China [80], have to be especially designed for those weather conditions. Problems that can occur during low temperatures are [182]:

Table 18

Comparison of energy amortisation time and emissions of various energy technologies. All figures include direct and indirect emissions based on average German energy mix, technology efficiency and lifetime. PV is based on average German solar radiation. The last column also includes methane emissions, based on CO₂-equivalent. N.A.=not considered in the relevant studies

Technology	Energy pay back time in months ^a	SO ₂ in kg/GWh ^a	NO _x in kg/GWh ^a	CO ₂ in t/GWh ^a	CO ₂ and CO ₂ equivalent for methane in t/GWh ^b
Coal Fired (pit)	1.0–1.1	630–1370	630–1560	830–920	1240
Nuclear	N.A.	N.A.	N.A.	N.A.	28–54
Gas (CCGT)	0.4	45–140	650–810	370–420	450
Large Hydro	5–6	18–21	34–40	7–8	5
Microhydro	9–11	38–46	71–86	16–20	N. A.
Smallhydro	8–9	24–29	46–56	10–12	2
Windturbine:					
4.5 m/s	6–20	18–32	26–43	19–34	N.A.
5.5 m/s	4–13	13–20	18–27	13–22	N.A.
6.5 m/s	2–8	10–16	14–22	10–17	11
Photovoltaic:					
Mono-cystalline	72–93	230–295	270–340	200–260	N.A.
Multi-cystalline	58–74	260–330	250–310	190–250	228
Amorphous	51–66	135–175	160–200	170–220	N.A.
Geothermal	N.A.	N.A.	N.A.	N.A.	50–70
Tidal	N.A.	N.A.	N.A.	N.A.	2

^a Source: Kaltschmitt et al. [132].

^b Source: Lewin [140], Fritsch et al. [109], for a summary of all studies in this field, see AWEA [74], for a similar Danish study see [169].

- brittle fracture of structural materials,
- insufficient lubrication of main bearings and generator bearings,
- excessive friction of gearbox,
- malfunctioning of hydraulics or electronics,
- icing of blades and meteorological sensors.

These problems may lead, among others, to long time stops without energy production. Icing on the blades can also result in ice throw which can constitute a significant public safety risk. Icing on the blades can have a significant impact on wind turbine performance, as it influences the blade aerodynamics as well as the blade load. According to simulations and experiments, icing reduces the standard deviation of the flapwise bending moment of the rotor blades, increases the standard deviation of the edgewise bending moment slightly, and also increases the fluctuations of the tower root bending moment significantly. The power spectral density of the edgewise bending moment has been found to increase by a factor of five of its natural frequency—indicating increased risk of edgewise vibrations [106].

Important features of extreme cold weather turbines are therefore heated anemometers as well as heated blades and probably heating systems for the safety system, gearbox and other items. For more details, see [104]

The research project “*Wind Energy Production in Cold Climates*”, WECO, which was partially supported by the European Commission DG XII’s Non Nuclear Energy Programme, studied related issues in detail. The project utilised simulation models as well as data obtained from existing cold weather projects in Finland. The results of this project are included in [106] as well as in [103, 104, 105, 111, 189]. The bi-annual BOREAS conference, organised by the Finnish Meteorological Institute usually presents the most recent research in the area of cold weather turbines.

Further cold weather research and projects exist in Canada as well as in the USA, see [80, 130, 133].

9.2. Offshore

The available area for wind energy development in central Europe, particularly in Germany, Denmark, the Netherlands, Great Britain and southern Sweden, is limited due to the high population density in these regions. National as well as Europe-wide studies found that offshore wind energy resources are significantly higher than onshore wind energy resources. Furthermore, in many central European waters the water depth increases only slowly with distance from shore [144], which is an important advantage for the utilisation of bottom-mounted offshore wind turbines. Therefore, large research projects have been set up to study the options for harvesting the offshore wind energy resources.

The main task of these research projects is to analyse the costs of developing offshore wind farms as well as to develop methods and wind turbine design which allows the installation, operation and maintenance of offshore wind farms. As maintenance of offshore wind turbines is particularly difficult and costly, special emphasis is put on approaches which require low maintenance [184].

Furthermore, offshore wind energy converters experience a complex loading due to dynamic changes of wind speed and direction as well as wave speed, height and direction. These complex loadings have to be taken into account for the structural design of offshore wind turbines. Research projects, therefore, focus on the wind turbine support structure, e.g. tower, as well as on the foundation. As the installation and supporting structure of offshore wind turbines is significantly more expensive than that of onshore turbines, offshore wind farms will have to use wind turbines with high rated capacity (≥ 1.5 MW) which are particularly designed for high wind speed sites and low maintenance (see e.g. [173]). An overview of the already existing offshore wind energy projects can be found in Table 7.

The most important studies regarding offshore have been, so far, *Study of Offshore Wind Energy in the EC* [144] and *Structural and Economic Optimisation of Bottom-Mounted Offshore Wind Energy Converters (Opti-OWECS)*. Opti-OWECS was a European research co-operation between different Universities as well as industrial companies. The results of the research project have been published in five final reports [88, 89, 90, 91, 92, 93] as well as in various conference reports, e.g. [134,

135, 136, 137] as well as in [138]. Another offshore wind energy study is dealing with cost optimisation of large projects, see [164]. The connection of wind parks via HVDC feeders, a likely possibility for offshore wind farms, is investigated in [18, 19, 175, 192].

The *Offshore Wind Energy Network* (see Section 11.1 for details) and the Conference on *Offshore Wind Energy in the Mediterranean and Other European Seas (OWEMOES)* [98] are also interesting information sources. In December 2001, the European Wind Energy Association (EWEA) held a special topic conference on offshore windpower in Brussels, Belgium. The proceedings will be soon available from the EWEA.

In addition, the project “*Concerted Action on Offshore Wind Energy in Europe*” (CA-OWEE) has set up a web page at: <http://www.offshorewindenergy.org> with very detailed reports on offshore wind power in download section.

9.3. Seawater desalination

Remote areas with potential wind energy resources such as islands can employ wind energy systems to power seawater desalination for fresh water production. The advantage of such systems is a reduced water production cost compared to the costs of transporting the water to the islands or to using conventional fuels as power source.

Different approaches for wind desalination systems are possible. First, both the wind turbines as well as the desalination system are connected to a grid system. In this case, the optimal size of the wind turbine system and the desalination system as well as avoided fuel costs are of interest. The second option is based on a more or less direct coupling of the wind turbine(s) and the desalination system. In this case, the desalination system is affected by power variations and interruptions caused by the power source (wind). These power variations, however, have an adverse effect on the performance and component life of certain desalination equipment. Hence, back-up systems, such as batteries, diesel generators, or flywheels might be integrated into the system. Main research in this area is related to the analysis of the wind plant and the overall system performance as well as to developing appropriate control algorithms for the wind turbine(s) as well as for the overall system.

Regarding desalination, there are different technology options, e.g. electro-dialysis or vapour compression. However, reverse osmosis is the preferred technology due to the low specific energy consumption.

The European Community, e.g. with the Joule III project, funded different research programs and demonstration projects of wind desalination systems on Greek and Spanish islands. For general information on wind desalination research, see [165, 100, 102]. For information on large stand-alone wind desalination systems, see [161, 162]; for small systems, see [118]; and for an overview of the research activities in North America, see [143].

9.4. *Small wind turbine systems*

Small wind turbine systems (≤ 10 kW) for electric power production are mainly used to supply remote, off-grid loads, such as homes, sailing boats, or telecommunication systems. Often they are used in combination with batteries and/ or small diesel generation systems.

The design of small wind turbine systems differs significantly from that of large, grid-connected wind turbines. Small wind turbines, for example, require different aerodynamic profiles to large wind turbines, due to different tip speed ratios. The wind energy industry, however, puts less emphasis on the development of aerodynamic profiles for small wind turbines than they have put on the development of aerodynamic profiles for large wind turbines. The aerodynamic performance of small-scale wind turbines is therefore significantly lower than that of larger wind turbines [128]. Research projects have been set up to develop more sophisticated aerodynamic profiles for small wind turbines, e.g. by the University of Newcastle/Australia (see Section 11.1).

Another difference between large and small wind turbines is the design of the transmission–generation system. Most small wind turbine systems are direct-driven, variable-speed systems with permanent magnet generators, hence a power converter is required to get a constant frequency if needed. Such a wind turbine design requires no gearbox. This approach is suitable for small wind turbines, as they operate with a much higher rotor speed than large wind turbines. This approach is also regarded as more reliable and less costly for maintenance. High reliability as well as low maintenance requirements are even more important for small wind turbines than for large ones, as maintenance and repair of single wind turbines in remote locations has an important impact on the overall economics of small wind turbines.

Also the power and speed regulation of small wind turbines vary significantly, e.g. mechanically controlled pitch systems or yaw systems instead of electronically controlled systems. Vertical and horizontal furling are also used for power control of small systems. In high winds, a vertical furling wind turbine will tilt the rotor skywards, giving the wind turbine the appearance of a helicopter. A horizontal furling turbine swings the rotor towards the tail during high wind speeds.

Both approaches are not used with larger wind turbines [128, 32]. Finally, small wind turbines have relatively tall towers in relation to the rotor diameter, as they need to get above near obstacles in the wind flow. Economically, small wind turbines are more expensive regarding the cost per kW than large wind turbines, however, they usually do not compete with grid electricity but with other forms of remote power supply, such as diesel generation or solar systems.

An excellent overview of design and operation of small wind turbines can be found in [32, 35, 36]; a comparison of different small wind turbines is provided in [167]. Reference [59] includes details for building a small wind turbine. Home Power Magazine [2] has regularly published articles about small wind systems.

9.5. Wind–diesel systems

For the power supply of small and medium-size, decentralised loads, e.g. remote villages, without connection to a grid, combinations of diesel generators and wind turbine have become an important alternative for a reliable and economic power supply. The total capacity of the wind–diesel system can thereby range from 50 kW to a few MW.

The wind–diesel system in the Australian city of Esperance, for example, includes eight diesel generators with a combined capacity of 14 MW and two wind farms with a combined capacity of 2.4 MW. It is reported that the system is capable of adequately responding to all power fluctuations, including wind power fluctuation, load fluctuations as well large fluctuations caused by lightning. At nights with low system loads and high wind speeds, the wind farms provide up to 75% of the total system load without problems [166].

Other examples can be found on the island of Crete and on Cape Verde. The island of Crete has a maximum demand of about 400 MW and no interconnection to the main grid. Currently, the installed wind capacity is 57.5 MW and a further 104 MW of wind power are planned. In Cape Verde, there are several wind–diesel systems. In the Sal and Mindelo power system, wind power has achieved a 14% penetration over a period of 3 years. Further wind projects are also planned on Cape Verde [84,96].

There are other projects all over the world. However, most projects are concentrated in countries with a low population density, e.g. Canada and Australia, or on islands.

Different design and control approaches for wind–diesel systems are used, e.g. often batteries are integrated in the system to supply power for up to 5 minutes to equalise the power output fluctuations of the wind turbine(s) and to avoid a brief start of the diesel generator(s). If the batteries run low, the diesel generator(s) starts up and feeds the load and recharges the batteries. The aim of this control strategy is to operate the diesel generator at high loads for most of the operation time, as this is the most fuel-efficient and therefore cost-efficient mode of operation.

In Denham, Western Australia, a wind–diesel–flywheel system is currently being tested. The system consists of three Enercon E30–230 kW wind turbines and two flywheels with an import–export rating of 400 kW (nominal)/600 kW (maximal) and an energy storage capacity of 10 kWh (at full import/export)/19 kWh at maximum. In addition, a 300 kVA synchronous compensator is connected so that the system can be operated without the diesel generator during times with high winds and moderate electricity demand. The project aims at supplying more than half of the electricity demand of Denham, reducing the annual diesel consumption by 450,000 litres [190].

The different alternatives for the operation and control of wind–diesel systems are presented in [30, 31], [55], pp. 58–59 and [194, 195] provide an overview of various publications in this field. The proceedings of the annual wind–diesel workshop contain recent research results [73]. For the simulation of wind–diesel systems, two simulation software packages are available on the Internet for free: The Hybrid Opti-

mization Model for Electric Renewables (HOMER) [151] and Hybrid2 [188], see also [195].

9.6. *Wind-pump systems*

The tradition of utilising wind energy for water pumping reaches back to the 1500s, e.g. the watering of potato plantations in the Cretan plateau of Lassithi, and the windpumps on cattle farms in the American Midwest. Today, in the industrialised countries wind energy is only scarcely utilised for water pumping. However, in developing countries, where many regions are not connected to an energy grid, the utilisation of wind energy constitutes an economical and environmentally friendly option for improving the water supply. In developing countries, the majority of the operating windpumps is currently applied for drinking-water supply and livestock watering. More recent approaches to use windpumps for irrigation have failed often due to the complexity of this application.

Water-pump systems can use a mechanical coupling of wind turbine and pump as well as an electrical one. From a wind energy perspective, electrical coupling of wind turbine and electrical pump can be regarded as a special application of small or medium-size wind turbines with a power generation unit.

As opposed to this, mechanical coupling of wind turbines and mechanical pumps requires wind turbines with a high number of blades in order to obtain a high starting torque. Different designs of windpump systems are used world-wide. Depending on the water location, e.g. underground water vs. surface water, the required pumping height and pumping volume, the water contamination and the available wind conditions, different pumps and different wind turbines can be used. Simple piston pumps, for instance, are often used in remote locations and eccentric screw pumps are currently tested in more advanced applications.

A wind-pump system with a mechanical coupling operates without a control mechanism, with the possible exception of an overspeed control at the wind turbine. A change in wind speed causes a direct change in the hydraulic data, particularly of the pumped volume flow rate. Hence, research focuses particularly on the engineering and efficiency issues of the overall system design but not system control issues.

For further discussions of wind-pump systems, see [32], engineering and efficiency issues are discussed in [30, 31], and [55], pp. 56–57 presents an overview of further publications.

10. Conclusions

Wind energy has the potential to play an important role in the future energy supply in many areas of the world. Within the last 12 years, wind turbine technology has reached a very reliable and sophisticated level. The growing world-wide market will lead to further improvements, such as large wind turbines or new system applications, e.g. offshore wind farms. These improvements will lead to further cost reductions

and over the medium term wind energy will be able to compete with conventional fossil fuel power generation technology. Further research, however, will be required in many areas, for example, regarding the network integration of a high penetration of wind energy.

11. Associations, research organisations and conferences

This section aims at providing contact details in the field of wind energy to keep up with the latest developments in the area.

Many of the following research organisations and some associations also offer workshops and courses for students, engineers and other interested individuals. The German Wind Energy Institute (DEWI), for example, offers a 6-months training course on wind energy technology for engineers from countries with a little experience in wind energy technology. Scholarships for this program are available from the German government. For more information, see the DEWI web-page: <http://www.dewi.de>.

11.1. Associations

This section lists associations with a major interest in wind energy. These organisations often organise and sponsor conferences and workshops and are also often involved in wind energy publications.

Agence de l'Environnement et de la Maitrise de l'Energie (ADEME), 27, rue Louis Vicat, F-75737 Paris Cedex 15, France, tel.: +33-01-47-65-20-00, fax: +33-01-46-45-52-36, e-mail: webmaster@ademe.fr, <http://www.ademe.fr>.

American Wind Energy Association (AWEA), 122 C Street, NW, 4th Floor, Washington, DC 20001, USA, tel.: +1-(202)-383-2500, fax: +1-(202)-383-2505, e-mail: windmail@awea.org <http://www.awea.org/> publishes Wind Energy Weekly and Windletter for its members. AWEA also offers a public Wind Energy Mailing List (awea-windnet@egroups.com), organises the yearly conference Windpower.

Association de pequenos productores y autogeneradores de electricidad con fuentes de energia renovables (APPAS), Dr Manuel de Delas, Paris, 205, E-08008 Barcelona, Spain, tel.: +34-93-4142277, fax: +34-93-2095307, e-mail: appa@adam.es.

Australian and New Zealand Solar Energy Society (ANZSES), ANZSES Administrator, PO Box 1140, Maroubra, NSW, 2035, Australia, tel.: +61-(0)2-9311-0003, fax: +61-(0)2-9311-0004, publishes the quarterly journal Solar Progress, organises the yearly conference Solar, e-mail: anzses@unsw.edu.au, <http://eureka.arch.unsw.edu.au/faculty/arch/solarch/anzses/anzses.htm>.

Australian Wind Energy Association (AusWEA), PO Box 432, 3840 Morwell VIC, Australia, tel.: +61-(3)-5133-6500, fax: +61-(3)-5133-6579, e-mail: info@auswea.com.au, <http://www.auswea.com.au>.

Austrian Wind Energy Association/IGW Interessengemeinschaft Windkraft Österreich, Mariahilfer Str. 89/22, A-1060 Wien, tel.: +43-(1)-5817060, fax: +43-(1)-5817061, e-mail: IGW@atmedia.net, <http://www.atmedia.net/IGW>.

British Wind Energy Association (BWEA), 26 Spring Street, London W2 1JA, UK, tel.: +44-(0)171-402-7102, fax: +44-(0)171-402-7107, e-mail: bwea@gn.apc.org, <http://www.bwea.com>, organises a yearly conference.

Canadian Wind Energy Association (CanWEA)/ L'association canadienne d'énergie éolienne, 3553 31 Street NW Suite 100, Calgary AB T2L 2K7, Canada, Toll Free phone in Canada: 1-800-9-CANWEA (1-800-922-6932), tel.: +1-403-289-7713, fax: +1-403-282-1238, e-mail: canwea@canwea.ca, <http://www.canwea.ca/indexen.htm>, organises a yearly conference as well as a wind-diesel workshop.

Danish Wind Turbine Manufacturers Association, Vester Voldgade 106, DK-1552 Copenhagen V, Denmark, tel.: +45-3373-0330, fax: +45-3373-0333, e-mail: danish@windpower.dk, <http://www.windpower.dk/core.htm> (the web page received the Poul la Cour Prize for outstanding contributions to the development of wind energy).

Danmarks Vindmølleforenings, Egensevej 24, 4840 Nr. Alslev, Denmark, tel.: +54-43-13 22, fax: +54-43-12-02, e-mail: info@danmarks-vindmoelleforening.dk, <http://www.danmarks-vindmoelleforening.dk>.

Dutch Wind Energy Association/Nederlandse Vereniging voor Windenergie (NEWIN), Postbus 1, 1755 ZG Petten, The Netherlands, tel.: +31-22464487, fax: +31-22463483.

European Wind Energy Association (EWEA), 26 Spring Street, London, W2 1JA, UK, tel.: +44-171-402-7122, fax: +44-171-402-7125, e-mail: ewea@ewea.org, <http://www.ewea.org>, publishes the quarterly journal Wind Directions.

Finnish Wind Power Association/Suomen Tuulivoimayhdistys Ry, PL 846, 00101 Helsinki, Finland, tel.: +358-(40)-56-19-765, <http://www.tuulivoimayhdistys.fi>.

Finnish Wind Energy Association/Vindkraftföreningen R.f., PB 124, FIN-65101 Vasa, Finland, tel.: +358-(0)500-862-886, fax: +358-(0)-6-312-8882, <http://www.vindkraftforeningen.fi>.

France Energie Eolienne, Institute Aerotechnique, 15 rue Marat, 78210 Saint Cyr L'école, France.

German Wind Energy Association/Bundesverband WindEnergie e.V., Herren-teichsstr. 1, 49074 Osnabrück, Germany, tel.: +49-(0)541-35060-0; fax: +49-(0)541-35060-30, e-mail: BWE—Os@t-online.de, <http://www.wind-energie.de/index.html>, publishes the monthly journal Neue Energien in German as well as the bimonthly journal New Energy in English.

Hellenic Wind Energy Association, Mr J Tsipouriois, 10 Ilias Street, chalandari 152 34, Athens, Greece, tel.: +30-1-603-9900, fax: +30-1-603 9905.

Indian Wind Turbine Manufacturers Association, tel.: +91-44-4899036, fax: +91-44-4899037, e-mail: DLWLMDS@giasmd01.VSNL.NET.IN.

International Solar Energy Society (ISES), ISES International Headquarters, Villa Tannheim, Wiesentalstr 50, D-79115 Freiburg i. Br., Germany, tel.: +49-(0)761-45906-0, fax. +49-(0)761-45906-99, e-mail: hq@ises.org,

<http://www.ises.org>, publishes the monthly journal *SunWorld Magazine*, and organises the bi-annual ISES Solar World Congress which usually includes sessions on wind energy.

Irish Wind Energy Association, Slane, County Meath, Ireland, tel./fax: +353-(0)41-982-6787, e-mail: staudt@iol.ie, <http://www.iwea.com>.

Japanese Wind Energy Association, c/o Japan Science Foundation, 2-1 Kitano-maru-koen Chiyodaku, Tokyo, Japan, tel.: +81-33212-8487, fax: +81-33212-0014, <http://ppd.jsf.or.jp/shinko/jwea>.

Kern Wind Energy Association, P.O. Box 277, Tehachapi, CA 93581, USA, tel.: +1-661-822-7956, fax: +1-661-831-3868, e-mail: kweawhite@aol.com, <http://www.kwea.org>, KWEA represents the wind industry in the Tehachapi–Mojave Wind Resource Area of Southern California.

National Wind Coordinating Committee (NWCC), c/o RESOLVE, 1255 23rd Street NW, Suite 275, Washington, DC 20037, free phone USA: +1(888)-764-WIND, tel.: +1-(202)-965-6398, fax: +1-(202)-338-1264, e-mail: nwcc@resolve.org, <http://www.nationalwind.org>.

Nederlandse Windenergie Vereniging, Secretariaat NEWIN, A.J. Brand, p/a ECN, Postbus 1, 1755 ZG Petten, e-mail: brand@ecn.nl, <http://www.newin.tmfweb.nl>.

New Zealand Wind Energy Association, c/o PO Box 388, Wellington, New Zealand, tel.: +64-4-5862003, fax: +64-4-5862004, e-mail: nzwea@wind-energy.org.nz, <http://www.windenergy.org.nz>.

Norsk Vindkraft Forum (NVF), Ola Flathus, Fasanenweg 13, D-25712 Burg, Germany, e-mail: ola.flathus@t-online.de.

Offshore Wind Energy Network, Co-ordinator Gillan Watson, Energy Research Unit, Rutherford Appleton Laboratory, Chilton, Didcot, Oxfordshire, OX11 0QX, UK, tel.: +44-(0)1235-446455, Fax.: +44-(0)1235-446863, e-mail: Gillian.Watson@rl.ac.uk, <http://www.owen.eri.rl.ac.uk/Default.htm>.

Society for the Promotion of Renewable Energies/Fördergesellschaft Erneuerbare Energien e.V., Innovationspark Wuhlheide, Köpenicker Str. 325, 12555 Berlin; Germany, tel.: +49-(0)30-65-76-27-06, fax: +49-(0)30-65-76-27-08, e-mail: FEE-eV@t-online.de; <http://www.FEE-eV.de>.

South African Wind Energy Association (SAWEA), PO Box 43286, Salt River, 7915, South Africa, tel./fax: +27-21-788-9758, e-mail: sawea@icon.co.za, <http://sawea.www.icon.co.za>.

Svensk Vindkraftförening, co Ordf Lennart Blomgren, Erikstorp Pl 7480, SE-533 92 Lundsbrunn, Sweden, tel.: +46-(0)-511-574-74, fax: +46-(0)-511-574-74, e-mail: info@svensk-vindkraft.org, <http://www.svensk-vindkraft.org>

Utility Wind Interest Group, 2111 Wilson Blvd., Suite 323, Arlington, VA 22201-3001, USA, tel.: +1-703-351-4492, ext.121, fax: +1-703-351-4495, <http://www.uwig.org>.

Vis Venti Poland, EPA Sp. z o.o., ul. Wojska Polskiego 154, 71-324 Szczecin, <http://www.elektrownie-wiatrowe.org.pl>.

World Renewable Energy Network, Professor Ali Sayigh, Director General of WREN, 147 Hilmanton, Lower Earley, Reading RG6 4HN, UK, tel.: +44-1189-

6111364, fax: +44-1189-611365, e-mail: asayigh@netcomuk.co.uk, <http://www.WRENUK.CO.UK>.

World Wind Energy Association, c/o Avenue de la Fauconnerie 73, 1170 Brussels, Belgium, e-mail: wwindea@wwindea.org, <http://www.wwindea.org>.

11.2. Research organisations

This section lists organisations that are involved in research on wind energy. Private companies are not listed, despite the fact that wind turbine manufacturers as well as consulting firms are also involved in wind energy research. See the Wind Energy Association Membership Lists for contact details of private companies. A list of US as well as international research centres can also be found in [55], pp. 107–114.

Aeronautical Research Institute of Sweden, Box 11021, Ranhammarsvägen 14, SE-161 11 Bromma, Sweden, tel.: +46-8-555-490-00, fax: +46-8-25-34-81, <http://www.ffa.se/>, publisher of Vindbladet.

CADDET—Centre for Renewable Energy, ETSU, Harwell, Oxfordshire OX11 0RA, UK, tel.: +44-1235-432719, fax: +44-1235-433595, e-mail: caddet.renew@aeat.co.uk, <http://www.caddet-re.org/html/wind.htm>.

Chalmers University of Technology, Department of Electric Power Engineering—Electrical Machines and Power Electronics, Hörsalsvägen 11, S-412 96 Göteborg, Sweden, tel.: +46-(0)31-772-1637, fax: +46-(0)31-772-1633, e-mail: ola.carlson@elkraft.chalmers.se, <http://www.elkraft.chalmers.se>.

Center for Renewable Energy Sources (CRES), Wind Energy Department, 19th klm. Marathonas Ave., GR-190 09 Pikermi, Greece, tel.: +30-1-6039900, fax: +30-1-6039905, <http://www.cres.gr/kape/index—uk.htm>.

Centre for Renewable Energy Systems Technology (CREST), AMREL Building (Angela Marmont Renewable Energy Laboratory), Loughborough University, LE11 3TU, UK, tel.: +44-1509-223466, fax: +44-1509-610031, <http://www.lboro.ac.uk/crest>.

Chinese Wind Energy Development Center, Huayan Rd. 3, Beijing 100083, VR China, tel.: +86-106202-0108, fax: +86-106201-2880.

Cranfield University, Wind Turbine Research Group, Cranfield, Bedford MK43 0AL, UK, Contact person: Richard L. Hales, tel.: +44-(0)1234-754640, fax: +44-(0)1234-750728, e-mail r.hales@cranfield.ac.uk, <http://www.cranfield.ac.uk/sme/ppa/wind>.

CSIRO Land and Water, Wind Energy Research Unit, Pye Laboratory, GPO Box 1666, Canberra, ACT 2601, Australia, e-mail: peter.coppin@cbr.clw.csiro.au, tel.: +61-(2)-6246-5576; fax: +61-(2)-6246-5560, <http://www.clw.csiro.au/research/environment/interactions>.

Delft University of Technology, Institute for Wind Energy, Faculty of Civil Engineering, Stevinweg 1, 2628 CN Delft, The Netherlands, tel.: +31-15-2785170, fax: +31-15-2785347, e-mail: ivw@CT.TUDELFT.NL, <http://www.ct.tudelft.nl/windenergy/ivwhome.htm>.

German Wind Energy Institute (DEWI)/ Deutsches Windenergie Institut,

Ebertstr. 96, D-26382 Wilhelmshaven, Germany, tel.: +49-(0)4421-4808-0, fax: +49-(0)4421-4808-43, e-mail: dewi@dewi.de, <http://www.dewi.de>, publisher of the quarterly journal DEWI Magazin (in German with English summaries), also organiser of the bi-yearly German Wind Energy Conference (DWEK), the conference usually takes place in the autumn of even years.

Institut für Solare Energieversorgungstechnik (ISET), Verein an der Universität Gesamthochschule Kassel, Königstor 59, D-34119 Kassel, Germany, tel.: +49-(0)561-7294-0, fax: +49-(0)561-7294-100, e-mail: mbox@iset.uni-kassel.de, <http://www.iset.uni-kassel.de/welcome.html>.

International Economic Platform for Renewable Energies/Internationales Wirtschaftsforum Regenerative Energien (IWR), Wind Energy Research Group, c/o Universität Münster, Robert-Koch-Str. 26–28, D-48149 Münster, Germany, tel.: +49-(0)251-83-33995, fax: +49-(0)251-83-38352, e-mail: iwr@uni-muenster.de, <http://www.iwr.de/wind/Welcomee.html>.

Iowa Wind Energy Institute, 1204 Lakeview Drive, Fairfield, IA 52556-9670, USA, tel.: +1-515-472-9828, fax: +1-515-472-9821, e-mail: tfactor@lisco.com.

Istanbul Technical University, Faculty of Aeronautics/Astronautics, Maslak, Istanbul, 80626, Turkey, tel.: +19-021-22-853-124, fax: +19-021-22-853-139, e-mail: tolun@itu.edu.tr.

Kocaeli University, Dr Tanay Sidki Uyar, Anitpark Yani, Izmit 41300, Kocaeli, Turkey, tel.: +90-262-3249947, fax: +90-262-3249909, e-mail: tanay@m-su.edu.tr.

National Renewable Energy Laboratory's National Wind Technology Center, 1617 Cole Boulevard, Golden, CO 80401-3393, USA, tel.: +1-(303)-384-6900, <http://www.nrel.gov/wind/index.html>.

National Technical University of Athens, Department of Mechanical Engineering, Fluid Section, Heroon Polytexneioy 9, Zografou campus, 157 73, Athens, Greece, tel.: +30-1-772-1056, fax: +30-1-772-1057, <http://www.fluid.mech.ntua.gr/wind/index.html>.

Netherlands Energy Research Foundation (ECN), P.O. Box 1, 1755 ZG Petten, The Netherlands, Contact: Bert Janssen, tel.: +31-224-564664, fax: +31-224-563214, e-mail: solar+wind@ecn.nl, <http://www.ecn.nl/unit—de/wind/main.html>.

Montana State University, College of Engineering, Wind Energy Program, 302 Cableigh Hall, Bozeman, MT 59717, USA, tel.: +1-406-994-4543, fax: +1-406-994-5308, e-mail: shelleyt@coe.montana.edu.

OSU Wind Research Cooperative, Department of Mechanical Engineering, Oregon State University, Corvallis, Oregon 97331-6001, USA, tel.: +1-541-737-2027, fax: +1-541-737-2600, e-mail: walkerst@engr.orst.edu, <http://www.me.orst.edu/WRC>.

Risø National Laboratory, Wind Energy & Atmospheric Physics Department, Building VEA-125, P.O. Box 49, DK-4000 Roskilde, Denmark, tel.: +45-4677-5000, fax: +45-4677-5970, e-mail: vea@risoe.dk, <http://www.risoe.dk/amv>.

Royal Institute of Technology (KTH), Department of Electric Power Engineering, Electric Power Systems, Teknikringen 33, SE-10044 Stockholm, Sweden,

tel.: +46-(0)8-790-8906, fax: +46-(0)8-7906510, e-mail: lennart.soder@ekc.kth.se, <http://www.ekc.kth.se>.

Rutherford Appleton Laboratory, Energy Research Unit, UK, Chilton, Didcot, Oxfordshire, UK OX11 0QX, tel.: +44-1235-445559, fax: +44-1235-446863, e-mail: J.A.Halliday@rl.ac.uk, <http://www.eru.rl.ac.uk>.

Sandia National Laboratory, New Mexico, PO Box 5800, Albuquerque, NM 87185, USA, e-mail: ashanse@sandia.gov, <http://www.sandia.gov/Renewable—Energy/wind—energy/homepage.html>.

Tata Energy Research Institute (TERI), Darbari Seth Block, Habitat Place, Lodhi Road, New Delhi 11 0003, India, tel.: +91-(0)11- 462-2246/4601550; fax: +91-(0)11-462-1770/463-2609, <http://www.teriin.org>.

Technical Research Centre of Finland (VTT), Energy/Energy Systems, Wind Energy, P.O.Box 1606, FIN-02044 VTT, Finland, tel.: +358-9-4561, fax: +358-9-456-6538, <http://www.vtt.fi/ene/enesys/AWP/info/info.html>.

Technical University Berlin, Aerospace Institute/Institut für Luft- und Raumfahrt, Workinggroup Windturbines, Sekr. F4, Marchstraße 12, D-10587 Berlin, Germany, tel.: +49-(0)30-314-22110, fax: +49-(0)30-314-79545, e-mail: wind@rotor.fb12.TU-Berlin.DE, <http://rotor.fb12.TU-Berlin.DE/engwindkraft.html>.

Technical University of Denmark, Department of Energy Engineering, Fluid Mechanics Section (AFM), Building 404, DTU, DK-2800 Lyngby, Denmark, tel.: +45-4593-2711, fax: +45-4588-2421, e-mail: afm@et.dtu.dk, <http://www.afm.dtu.dk/wind>.

University of Massachusetts, Renewable Energy Research Laboratory, College of Engineering, E lab Building, Amherst, MA 01003, tel.: +1-413-545-4359, fax: +1-413-545-1027, e-mail: manwell@ecs.umass.edu, Web site: <http://www.ecs.umass.edu/mie/labs/rerl>.

University of Newcastle, Department of Mechanical Engineering, Wind Energy Group, University Drive, Callaghan NSW 2308, Australia, tel.: +61-(2)-4921-6200, fax: +61-(2)-4921-6946, <http://www.eng.newcastle.edu.au/me/wind/#mem>.

University of Utah, Mechanical Engineering, Wind Energy Research Group, 50 S. Central Campus Drive, Room 2202, Salt Lake City, Utah 84112-9208, USA, tel.: +1-(801)581-6441; fax: +1-(801)585-982, <http://www.cc.utah.edu/~djl3109/windhome.html>.

11.3. Conferences

Conferences are the best way to keep up to date regarding developments in the fast moving field of wind energy technology. Most wind energy associations as well as research organisations regularly organise conferences or workshops. The following conferences attract most international attention and usually publish conference proceedings (contact details of the organisers can be found in Sections 11.1 and 11.2):

Yearly:

- Windpower Conference, organised by the American Wind Energy Association, yearly;

- Wind-Diesel Workshop, jointly organised by the Canadian Wind Energy Association and the American Wind Energy Association;
- British Wind Energy Association Conference, yearly;
- International Workshop on Feasibility of HVDC Transmission Systems for Off-shore Wind Farms, organised by the Royal Institute of Technology, Stockholm, Sweden.

Bi-annual:

- European Wind Energy Conference, sponsored by the European Wind Energy Association, usually the largest wind energy event world-wide with very good proceedings;
- German Wind Energy Conference, organised by the German Wind Energy Institute;
- World Wind Energy Conference; in 2002, two world wind events will take place, the 2002 Global Wind Power Conference and Exhibition, 2–5 April 2002, Paris, France, organised by the European Wind Energy Association and the World Wind Energy Conference and Exhibition, 2–6 July 2002, Berlin, Germany, organised by the German Wind Energy Association (BWE). It is, however, planned to combine those events in the future.
- BOREAS Conference, organised by the Finnish Meteorological Institute;
- World Renewable Energy Conference, organised by the World Renewable Energy Network.

Three-yearly:

- Offshore Wind Energy in the Mediterranean and Other European Seas (OWEMOES), organised by ENEA, Roma, Italy.

Four-yearly:

- International Conference on Wind Engineering, organised by International Association for Wind Engineering.

The following Internet links provide further information regarding upcoming wind energy events:

- Wind Power Monthly: <http://www.windpower-monthly.com/calendar.htm>,
- National Wind Coordinating Committee: <http://www.nationalwind.org/events/default.htm>,
- Renewable Energy Meeting Calendar: <http://www.ttcorp.com/calendar.htm>.

12. About the bibliography

12.1. Periodicals

Most wind energy associations as well as some research organisations have regular publications available that are dedicated to wind energy. See the previous section for details. The references [1]–[13] provide an overview of additional publications that are solely related to wind energy or that regularly feature articles on this topic. These periodicals are an important source of news and developments in the wind energy research and industry. For another useful overview of wind energy periodicals, see [55], pp. 102–106.

12.2. Wind energy resources

Wind resource studies were carried out in many countries. In many cases, however, the analysed wind data is obtained from existing wind measurement stations, for example located at airports. Hence, the wind resource studies are only useful to obtain a general impression of the wind distribution. Further wind measurements are always necessary to validate the available wind resources, see also [158, 157, 30, 31].

In [14] and [15], two examples of good wind resource atlas are given; [16] and [17] are two wind energy resource research organisations. Most research organisations mentioned in Section 11.2 also work in the field of wind energy resources. For an overview of wind energy resource publications, see [55], pp. 17–19.

12.3. Books

References [18–67] are books and proceedings available in the area of wind energy.

The Danish Wind Turbine Manufacturers Association operates a web page at www.windpower.dk that provides an excellent introduction into the basics of wind energy technology. The webpage is available in three languages, English, German, Danish, some sections also in Chinese and French. Other books are listed in references [18]–[67].

12.4. Bibliographies

In [68], the most recent bibliographies that focus on wind energy or feature sections on wind energy are listed. The Wind Energy Information Guide by the National Renewable Energy Laboratory contains a list of wind energy bibliographies published before 1996 as well as a list of bibliographic databases that contain information on wind energy, [55], pp. 94–100. Wind Energy [10] has started to regularly publish a wind energy literature survey, [10], 2000, issue 3, pp. 165–166 and 2001, issue 1, pp. 39–41/.

12.5. *Studies/Articles*

References [69–191] provide details of studies and articles in this field.

12.6. *Glossary*

Gipe and Carter have published the largest glossary on wind energy terms, see [34].

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References

Periodicals

- [1] EWTS bulletin, a sixmonthly newsletter of the European Wind Turbine Standards (EWTS) project, published by ECN-Renewable Energy, Petten, the Netherlands, see also: <http://www.awea.org/tech/ewts/index.html>.
- [2] Home Power magazine, regularly publishes articles on small wind energy systems, PO Box 520, Ashland, OR 97520 USA, tel.: +1-541-512-0201, fax: +1-530-475-0836, e-mail: hp@home-power.com, <http://www.homepower.com>.
- [3] IEA Wind Energy Annual Report, published by International Energy Agency (IEA), Paris, France.
- [4] Journal of Wind Engineering and Industrial Aerodynamics, technical journal on wind effects, published since 1975, ISSN: 0167-6105, Elsevier Science.
- [5] Renewable Energy, the official journal of WREN—The World Renewable Energy Network, published since 1985, ISSN: 0960-1481, Elsevier Science.
- [6] Renewable Energy World, a six-monthly free industry magazine, ISSN: 1462-6381, James & James, London, UK.
- [7] Windmills' Gazette, quarterly newsletter on American windmill restoration, contact T. Lindsay Baker, Windmills' Gazette, P.O. Box 507, Rio Vista, Texas 76093, USA.
- [8] Windpower Monthly, industry magazine, monthly, published since 1985, ISSN 0901-7318, PO Box 100, DK-8420 Knebel, Denmark, tel.: +45-8-636-5465, fax: +45-8-636-5626, e-mail: mail@windpower-monthly.com, <http://www.windpower-monthly.com>.
- [9] WindStats Newsletter, industry magazine with world-wide statistical data on wind turbine performance, published since 1987, PO Box 100, DK-8420 Knebel, Denmark, tel.: +45-8-636- 5900, fax: +45-8-636-5626, e-mail: windstats@forlaget-vistoft.dk, <http://www.windstats.com>.
- [10] Wind Energy, technical journal, published four times a year since 1998, ISSN 1095-4244, John

Wiley & Sons, Ltd, Baffins Lane, Chichester, West Sussex PO19 1UD, UK, see also: <http://www.interscience.wiley.com/jpages/1095-4244/>.

- [11] Wind Energy Newsletter, published semi-annually by International Energy Agency (IEA), Paris, France.
- [12] Wind Engineering, technical journal, Multi-Science Publishing, 107 Hight St, Brentwood, Essex CM14 4RX, UK, tel.: +44-277-224632, fax: +44-277-223453.
- [13] Wind Kraft Journal and Natürliche Energien, German bimonthly industry journal with operation data from German wind turbines, Verlag Natürliche Energien, D-24811 Brekendorf, Tirol, tel.: +49-(0)4353-551, fax: +49-(0)4353-796.

Wind Atlas

- [14] Europe: European Wind Atlas, published by the Risø National Laboratory, Roskilde, Denmark, for the European Commission.
- [15] USA: Wind Energy Resource Atlas of the United States, by the Pacific Northwest National Laboratory, available on the web at <http://redc.nrel.gov/wind/pubs/atlas/atlas—index.html>, distributed by the American Wind Energy Association.

Research

- [16] Finland: Finnish Meteorological Institute, Meteorological Research, Vuorikatu 24, P.O. Box 503, 00101 Helsinki, Finland, tel.: +358-9-1929-4101, fax. +358-9-1929-4103, <http://www.fmi.fi/TUT/MET/energia/ene—engl.html>.
- [17] OSU Energy Resources Research Laboratory, Department of Mechanical Engineering, Oregon State University, Corvallis, Oregon 97331-6001, tel.: +1-541-737-2027, fax: +1-541-737-2600, e-mail: walkers@ccmail.orst.edu, <http://www.me.orst.edu/ERRL/>.

Books

- [18] Ackermann T, Jones L, editors. Proceedings of the First International Workshop of HVDC Transmission Networks for Offshore Wind Farms, March 2000, Royal Institute of Technology, Electric Power Systems, Stockholm, Sweden.
- [19] Ackermann T, editor. Proceedings of the Second International Workshop on Transmission Networks for Offshore Wind Farms, March 2001, Royal Institute of Technology, Electric Power Systems, Stockholm, Sweden.
- [20] Asmus P. Reaping the wind: how mechanical wizards, visionaries, and profiteers helped shape our energy future. Washington, USA: Island Press, 2000.
- [21] Baker LT. A field guide to American windmills, University of Oklahoma Press, Norman, OK, USA, 1985.
- [22] Betz A. Windenergie und ihre Ausnutzung durch Windmühlen. Vandenhoeck & Ruprecht, Göttingen 1926. Reprint by Öko-Verlag Kassel, Germany, 1982.
- [23] Burton T, Sharpe D, Jenkins N, Bossanyi E. Wind energy handbook. Chichester, UK: J. Wiley & Sons, 2001.
- [24] DEWI: Wind Energy Information Brochure; published by German Wind Energy Institute (DEWI), Wilhelmshaven 1998, available in English and in Spanish.
- [25] Dörner H. Drei Welten—Ein Leben Professor Dr Ulrich Hütter. Stuttgart, Germany: Institut für Flugzeugbau (IFB), Universität Stuttgart, 1995.
- [26] Eggleston S. Wind turbine engineering design. New York, USA: van Nostrand Reinhold Company, 1987.
- [27] Energie Verwertungsagentur: Feed-in tariffs and regulations concerning renewable energy electricity generation in European countries; Vienna, Austria, August 98, available at: <http://www.eva.wsr.ac.at/publ/dl.htm>.

- [28] Wind energy—the facts. European Commission, Directorate-General for Energy, 1998; available at <http://www.ewea.org/information.htm>.
- [29] Freris LL. Wind energy conversion systems. Hertfordshire, UK: Prentice Hall International, 1990.
- [30] Gasch, R. Windkraftanlagen. In Gasch R, Teubner BG, editors. 3rd ed. Stuttgart, Germany (German version of Wind turbine generators).
- [31] Gasch R. Wind power plants—fundamentals, design, construction and operation, to be published by Solarpraxis, Berlin, June 2002, distributed by German Wind Energy Association.
- [32] Gipe P. Wind power for home & business. White River Junction, VT: Chelsea Green Publishing Co, 1994.
- [33] Gipe P. Wind energy comes of age. USA: J. Wiley & Sons, 1995.
- [34] Gipe P, Canter B. Glossary of wind energy terms. Denmark: Forlaget Vistoft, 1997.
- [35] Gipe P. Wind energy basics—a guide to small and micro wind systems. White River Junction, VT: Chelsea Green Publishing Co, 1999.
- [36] Gipe P. Energía Eólica Práctica. Progensa, Seville, Spain, 2000. Spanish translation of Wind energy basics—a guide to small and micro wind systems.
- [37] Johansson Thomas B, Kelly Henry. Renewable energy sources for fuels and electricity. Island Press, Washington, USA, 1993.
- [38] Grubb MJ, Meyer NI. The generation of electricity by wind power. New York, USA: J. Wiley & Sons, 1976.
- [39] Grubb M, Vigotti R. Renewable energy strategies for Europe—electricity systems and primary electricity sources, vol. 2. London, UK: The Royal Institute of International Affairs, 1997.
- [40] Hansen MOL. Aerodynamics of wind turbines. London, UK: James & James, 2001.
- [41] Harrison R, Hau E, Snel H. Large wind turbines: design and economics. J. Wiley & Sons, 2001.
- [42] Hau E. Windkraftanlagen. Berlin/Heidelberg, Germany: Springer Verlag, 1988.
- [43] Hau E. Windturbines—fundamentals, technologies, application, economics. Berlin/Heidelberg, Germany: Springer Verlag, 2000.
- [44] Heier S. Windkraftanlagen im Netzbetrieb., 2nd ed Stuttgart, Germany: B.G. Teubner, 1996 German version of Grid integration of wind energy conversion systems.
- [45] Heier S. Grid integration of wind energy conversion systems. Chichester, UK: J. Wiley & Sons, 1998.
- [46] Heymann, M. Die Geschichte der Windenergienutzung 1890–1990 (The history of wind energy utilization 1890–1990), Campus Verlag, Frankfurt am Main, Germany, 1995.
- [47] Hills RL. Power from wind—a history of windmill technology. Cambridge, UK: Cambridge University Press, 1994.
- [48] Hojstrup J, Tammelin B. Wind resources in complex terrain. Riso—Contribution from the Department of Meteorology and Wind Energy to the EUWEC'96 Conference in Goeteborg, Sweden. Larsen GC, editor. Riso National Laboratory, Roskilde, Denmark, August 1996, pp. 15–18.
- [49] Jahresauswertung 1997 des wissenschaftlichen Mess- und Evaluierungsprogramm zum Breitentest “250 MW Wind” (Statistical analysis of the German scientific measurement and evaluation programme “250 MW Wind”, published yearly by Institut für Solare Energieversorgungstechnik (ISET), Kassel, Germany, <http://www.iset.uni-kassel.de:888>.
- [50] IEA Wind Energy Annual Report 2000, published by International Energy Agency/ OECD, Paris, May 2001.
- [51] Johnson GL. Wind energy systems. New York, USA: Prentice Hall, 1985.
- [52] Kealey EJ. Harvesting the air: windmill pioneers in twelfth-century England. Berkeley, CA: University of California Press, 1987.
- [53] Koepl GW. Putnam's Power from the wind. 2nd ed. New York: Van Nostrand Reinhold Company, 1982.
- [54] Molly J-P. Windenergie., 2nd ed Karlsruhe, Germany: C.F. Müller, 1990.
- [55] Wind energy information guide. Published by the US Department for Energy, produced by the National Renewable Energy Laboratory, DOE/GO-10095-258, DE96000474, available from NTIS, US Department of Commerce, 5285 Port Royal Road, Springfield, VA 22161, USA, 1996.
- [56] Nielsen FB. Wind turbines & the landscape: architecture & aesthetics. Prepared for the Danish Energy Agency's Development Programme for Renewable Energy, ISBN 87-985801-1-6, 63 pages,

Originally appeared as *Vindmøller og Landskab: Arkitektur og Æstetik*, ISBN 87-985-801-0-8; Denmark, 1996.

- [57] Fifth renewable order for England and Wales. Office of Electricity Regulation, UK, September 1998, available at: <http://www.open.gov.uk/offer/offerhm.htm>.
- [58] Pasqualetti M, Gipe P, Righter R. Wind power in view—energy landscapes in a crowded world. San Diego, CA: Academic Press, 2002.
- [59] Piggott H. Windpower workshop. Centre for Alternative Technology Publications, 1982. ISBN 1-898049-13-0, 158 pp. (CAT Publications, Powys, Wales, UK, May 1997).
- [60] Putnam PC. Power from the wind. 224 pp., Van Nostrand, New York, 1948 (reprinted 1974).
- [61] Shepherd DG. Historical development of the windmill. US Department of Energy (DOE/NASA-5266-2), Washington, DC, December 1990.
- [62] Söder L. Vindkraftens effektivvärde (Capacity credit of wind power, in Swedish); Elforsk Rapport 97:27, Stockholm, Sweden, December 1997.
- [63] Spera DA. Wind turbine technology. New York, USA: ASME Press, 1994.
- [64] Stanton C. The landscape impact and visual design of windfarms. Edinburgh, Scotland: School of Landscape Architecture, 1996.
- [65] Righter R. Wind energy in America: a history. Norman, OK: University of Oklahoma Press, 1996.
- [66] Wagner S, Bareiß R, Guidati G. Wind turbine noise. Berlin/Heidelberg, Germany: Springer-Verlag, 1996.
- [67] Walker JF, Jenkins N. Wind energy technology. Chichester, UK: J. Wiley & Sons, 1997.

Bibliographies

- [68] On-line bibliography, see <http://www.nrel.gov/wind/wind—bib.html>.

Studies/Articles

- [69] Ackermann T, Andersson G, Söder L. Overview of government and market driven programs for the promotion of renewable power generation. Proceedings of the World Renewable Energy Congress, 10th to 13th February 1999, Perth, Australia.
- [70] Ackermann T, Garner K, Gardiner A. Wind power generation in weak grids—economic optimisation and power quality simulation. *Renewable Energy* 1999;18(2):205–21.
- [71] Akhmatov V, Knudsen H. Modelling of windmill induction generators in dynamic simulation programs. Proceedings of the IEEE Power Technical Conference, 1999, Budapest, Hungary.
- [72] Wind energy technical standards. Eight different standards documents, published by the American Wind Energy Association, see also: <http://www.awea.org/standards/index.html>.
- [73] Wind—diesel workshop proceedings, published yearly by the Canadian Wind Energy Association/American Wind Energy Association, see also: <http://www.awea.org/pubs/wd.html>.
- [74] Energy and emission balance favours wind. *Wind Energy Weekly* #521, published by American Wind Energy Association, USA, 9 November 1992.
- [75] Ancona DF. Power generation, wind ocean. In: Wilk's encyclopedia of architecture, design, engineering and construction, vol. 4. New York: J. Wiley & Sons; 1989. p. 32–9.
- [76] Barthelmie RJ, Mortensen NG, Landberg L, Hojstrup J. Application of the WAsP model to determine the wind resource in non-neutral conditions in coastal areas. Riso—Contribution from the Department of Meteorology and Wind Energy to the EUWEC'96 Conference in Goeteborg, Sweden, Larsen GC, editor. Riso National Laboratory, Roskilde, Denmark, August 1996, pp. 27–30.
- [77] Bergeles G, Glekas I, Prospathopoulos I, Voutsinas S. Statistical and physical modelling of wind resources in complex terrain: assessment of the applicability of a 3D Navier–Stokes Code. Proceedings of the 1996 European Wind Energy Conference, 20–24 May 1996, Goeteborg, Sweden, pp. 560–563.
- [78] Bossanyi E, Saad-Saoud Z, Jenkins N. Prediction of flicker produced by wind turbines. *Wind Energy* 1999;2(1):35–51.
- [79] Bowen AJ, Mortensen NG. Exploring the limits of WAsP—the wind atlas analysis and application program. Riso—Contribution from the Department of Meteorology and Wind Energy to the

- EUWEC'96 Conference in Goeteborg, Sweden, Larsen GC, editor. Riso National Laboratory, Roskilde, Denmark, August 1996, pp. 23–26.
- [80] Bright D, Salaff S. Designing for arctic survival. *Windpower Monthly* 1996;12(6):42–5.
- [81] Bruntt M, Havsager J, Knudsen H. Incorporation of wind power in the east Danish power system. Proceedings of the IEEE Power Technical Conference 1999, Budapest, Hungary.
- [82] Carlson O, Grauers A, Svensson J, Larsson Å. A comparison between electrical systems for variable speed operation of wind turbines. Proceedings European Wind Energy Conference 1994, Thessaloniki, Greece, 10–14 October 1994, pp. 500–505.
- [83] Christensen JF, Sorensen AG, Hatziaargyriou N, Donnelly M. Methods and models for evaluating the impact of decentralized generation. CIGRE (International Conference on large High Voltage Electric Systems), Session 1998, Paper presented on behalf of Study Committee 38, Paris, 1998.
- [84] Craig L, Gardner P. Network quality and power system operation with high wind energy penetration. UK: British Wind Energy Association, 1998.
- [85] Crespo A, Hernández J, Frandsen S. Survey of modelling methods for wind turbine wakes and wind farms. *Wind Energy* 1999;2(1):1–24.
- [86] Croba D, Tryfonopoulos D, Casanova M, Martin B, Morgana B, Rodrigues A, Schmid J, Voutsinas S. Improving techniques for statistical and physical modelling of wind resources in complex terrain; Proceedings of the 1996 European Wind Energy Conference, 20–24 May 1996, Goeteborg, Sweden, pp. 514–517.
- [87] Davitian H. Wind power and electric utilities: a review of the problems and prospects. *Wind Engineering*, vol. 122, 1978.
- [88] Opti-OWECS final report: structural and economic optimisation of bottom-mounted offshore wind energy converters—vol. 0: Executive summary; EU Joule III Project JOR3-CT95-0087, published by Delft University of Technology, ISBN 90-76468-01-X, the Netherlands, August 1998, 40 pages; information available at: <http://www.ct.tudelft.nl/windenergy/owecs/title.htm>.
- [89] Opti-OWECS final report—vol. 1: integrated design methodology for offshore wind energy conversion systems; EU Joule III Project JOR3-CT95-0087, published by Delft University of Technology, ISBN 90-76468-02-8, the Netherlands, August 1998, 94 pages.
- [90] Opti-OWECS final report—vol. 2: methods assisting the design of offshore wind energy conversion systems; EU Joule III Project JOR3-CT95-0087, published by Delft University of Technology, ISBN 90-76468-03-6, the Netherlands, August 1998, 226 pages.
- [91] Opti-OWECS final report—vol. 3: comparison of cost of offshore wind energy at European sites; EU Joule III Project JOR3-CT95-0087, published by Delft University of Technology, ISBN 90-76468-04-4, the Netherlands, August 1998, 86 pages.
- [92] Opti-OWECS final report—vol. 4: a typical design solution for an offshore wind energy conversion system; EU Joule III Project JOR3-CT95-0087, published by Delft University of Technology, ISBN 90-76468-05-2, the Netherlands, August 1998, 274 pages.
- [93] Opti-OWECS final report—vol. 5: user guide OWECS cost model; EU Joule III Project JOR3-CT95-0087, published by Delft University of Technology, ISBN 90-76468-06-0, the Netherlands, August 1998, 46 pages.
- [94] Diez Castro A, Ellström R, Ying JH, Christer L. Co-ordination of parallel AC–DC systems for optimum performance. Proceedings of DistribuTECH, 28–30 September, Madrid, Spain, 1999.
- [95] Penetration of wind energy in Ireland; Econnect, 2000; available at: <http://www.iwea.com/publications/index.html>
- [96] High penetration of wind energy in the Cape Verds Islands; Electra, 1995; available at: <http://www.inforse.dk/cases/capeverd.html>.
- [97] Wind Turbine Verification Program (TVP), sponsored by US Department of Energy and the Electric Power Research Institute (EPRI), plans to publish regular status reports. The first one, 1998 Status Report on TVP (MI 112231), can also be found at <http://hubub.epri.com/gg/renew/tvp/tvp.html>.
- [98] Proceedings of the Offshore Wind Energy in the Mediterranean and Other European Seas Conference, 1997, at La Maddalena island, Sardinia, Italy; published by ENEA Casaccia Research Center, S. Maria di Galeria (Rome), Italy 1997.
- [99] Eppel DP, Kapitza H, Claussen M, Jacob D, Koch W, Levkov L, Mengelkamp H-T, Werrmann

- N. The non-hydrostatic mesoscale model GESIMA. Part II: Parameterizations and applications, *Beiträge zur Physik der Atmosphäre*, February 1995, 15–41.
- [100] Desalination guide using renewable energies. Maxibrochure under THERMIEDG XVII published by C.R.E.S. Centre for Renewable Energy Sources, Pikermi-Attiki, Greece, 1998.
- [101] Wind force 10—a blueprint to achieve 10% of the world's electricity from wind power by 2020. Published by the European Wind Energy Association, London, UK, Forum for Energy and Development, Copenhagen, Denmark and Greenpeace International.
- [102] Feron P. Use of windpower in autonomous reverse osmosis seawater desalination. *Wind Engineering* 1985;9(3):180–99.
- [103] Proceedings of BOREAS III, 19–21 March 1996 in Saariselkä, Finland, published by the Finnish Meteorological Institute, Helsinki, Finland, 1996.
- [104] Proceedings of BOREAS IV, published by the Finnish Meteorological Institute, Helsinki, Finland, 1999.
- [105] Proceedings of BOREAS V, published by the Finnish Meteorological Institute, Helsinki, Finland, 2001.
- [106] Final report of the “Wind Energy Production in Cold Climates”, WECCO, research project; to be published by the Finnish Meteorological Institute, Helsinki, Finland and the European Commission DG XII, 1999/2000; for further information, see <http://www.fmi.fi/TUT/MET/energia/wecocontents.html>.
- [107] The European Wind Energy Association Special Topic Conference on the Economics of Wind Energy; Proceedings published by Finnish Wind Power Association, Helsinki, 1995, see also: <http://rotor.fb12.tu-berlin.de/windnet/EWEAeconomics95.html>.
- [108] Flay RGJ, Phillips DG, Richards PJ. Development of diffuser augmented wind turbine designs in New Zealand. In: Proceedings of the European Wind Energy Conference, Nice, France, March. James & James; 1999. p. 349–52.
- [109] Fritsch et al., Umweltwirkungsanalyse von Energiesystemen, Gesamt-Emissions-Modell integrierter Systeme; Hessisches Ministerium für Wirtschaft und Technology, Wiesbaden, Germany, 1989.
- [110] TERNA-Studie: “Energiewirtschaftliche Rahmenbedingungen und Anreizsysteme für netzgekoppelte Stromproduktion aus erneuerbaren Energien”; published by: Deutsche Gesellschaft für Technische Zusammenarbeit (GTZ)—German Technical Cooperation, Eschborn, Germany.
- [111] Proceedings of WOWECO II (Wind Energy Production in Cold Climates) Workshop in Wilhelmshaven, Germany; published by: German Wind Energy Institute—Deutsches Windenergie Institute (DEWI), Wilhelmshaven, Germany, June 1997.
- [112] Hannah P, Warren JG. Comparison of windspeed modelling techniques at existing and potential wind farm sites across the UK. Proceedings of the 1995 Seventeenth BWEA (British Wind Energy Association) Conference, pp. 199–204.
- [113] Heier S. Anschluss von Windkraftanlagen an das öffentliche Netz. *Sonnenenergien & Wärmetechnik* 1997;3:44–51.
- [114] Milligan MR. Modelling utility-scale wind power plants. Part 1: Economics. *Wind Energy* 1999;2(4):167–93.
- [115] Milligan MR. Modelling utility-scale wind power plants. Part 2: Capacity credit. *Wind Energy* 2000;3(4):167–206.
- [116] Hirsch W, Rindelhardt U, Tetzlaff G. Saxon wind energy resources: comparison of WASP and KAMM results. Proceedings of the 1996 European Wind Energy Conference, 20–24 May 1996, Goeteborg, Sweden, pp. 604–607.
- [117] Hojstrup J, Tammelin B. Wind resources in complex terrain. Riso—Contribution from the Department of Meteorology and Wind Energy to the EUWEC'96 Conference in Goeteborg, Sweden, Larsen GC, editor. Riso National Laboratory, Roskilde, Denmark, August 1996, pp. 15–18.
- [118] Infield D. Performance analysis of a small wind powered reverse osmosis plant. *Solar Energy* 1997;61(6):415–21.
- [119] International Electrotechnical Commission: <http://www.iec.ch>.
- [120] International Electrotechnical Commission: IEC Standard, Publication IEC 61000-4-7, 1991.
- [121] International Electrotechnical Commission: IEC Standard, Publication IEC 61800-3, 1996.

- [122] International Electrotechnical Commission: Wind turbine generator systems—Part 11: Acoustic noise measurement techniques. IEC Standard, Publication IEC 61400-11, 1998.
- [123] International Electrotechnical Commission: Wind turbine generator systems—Part 12: Wind turbine power performance testing. IEC Standard, Publication IEC 61400-12, 1998.
- [124] International Electrotechnical Commission: Wind turbine generator systems—Part 2: Safety of small wind turbines. IEC Standard, Publication IEC 61400-2, 1996. VERSION OFICIAL EN ESPANOL—Aerogeneradores. Parte 2: Seguridad de los aerogeneradores pequeños. IEC Standard, Publication IEC 61400-2, 1996.
- [125] International Electrotechnical Commission: International electrotechnical vocabulary—Part 415: Wind turbine generator systems. IEC Standard, Publication IEC 60050-415, 1999.
- [126] International Electrotechnical Commission: Wind turbine generator systems—Part 1: Safety requirements. IEC Standard, Publication IEC 61400-1, 1999.
- [127] International Energy Agency: Electricity information 1997. Published by International Energy Agency/OECD, Paris 1998.
- [128] Jamieson, P., Design challenges for growing sector. *Wind Directions*, April (1998), XVII(3), 16–17.
- [129] Jamieson, P., Small wind turbines—the market. *Wind Directions*, April (1998), XVII(3), 16–17.
- [130] Jasinski WJ, Noe SC, Selig MS, Bragg MB. Wind turbine performance under icing conditions. *Transactions of the ASME*, 120, February 1998.
- [131] Jensen NO. Atmospheric boundary layers and turbulence; in: *Proceedings of the Tenth International Conference on Wind Engineering*, Copenhagen, Denmark, June 1999, vol. 1, pp. 29–42, ISBN 9058090590.
- [132] Kaltschmitt M, Stelzer T, Wiese A. Ganzheitliche Bilanzierung am Beispiel einer Bereitstellung elektrischer Energie aus regenerativen Energien; in *Zeitschrift für Energiewirtschaft*, vol. 20; Heft 2, 1996; *Energiewirtschaftliches Institute an der Universität Köln*, Germany 1996, pp. 177–178.
- [133] Kotzebue Electric Association 1999. A description of the cold climate wind plant in Kotzebue, Alaska, USA is available at: <http://www.eren.doe.gov/wind/kotzebue.html> as well as <http://www.kotzelectric.com/wind/wind—home.html>.
- [134] Kühn M. et al., editors. Structural and economic optimisation of offshore wind converters—overview of second phase of the Joule III Project Opti-OWECS; in: *Proceedings of European Seminar: Offshore Wind Energy in Mediterranean and other European Seas (OWEMES '97)*, Sardinia, Italy, April 1997; also *Wind Engineering*, vol. 21 (4) 1997; and available at: <http://www.ct.tudelft.nl/windenergy/publicat.htm#IPp99>.
- [135] Kühn M. et al., editors. Dynamics of offshore wind converters—contribution to the Joule III Project Opti-OWECS; in: *Proceedings of European Seminar: Offshore Wind Energy in Mediterranean and other European Seas (OWEMES '97)*, Sardinia, Italy, April 1997; also *Wind Engineering*, vol. 21 (3) 1997; and available at: <http://www.ct.tudelft.nl/windenergy/publicat.htm#IPp99>.
- [136] Kühn M, Bierbooms, W. Offshore wind energy—a future market under rapid development; published by the Delft University of Technology, Institute for Wind Energy, the Netherlands, 1998, available at: <http://www.nemesis.at/publication/gpi—98—2/articles/56.html>
- [137] Kühn M et al. Towards a mature offshore wind energy technology—guidelines from the opti-OWECS project. *Wind Energy* 1999;2(1):25–58.
- [138] Kühn M. Dynamics and design optimisation of offshore wind energy conversion systems. Ph.D. thesis, Delft University Wind Energy Research Institute, Report 2001.002.
- [139] Landberg L, Mortensen NG, Petersen EL. Wind resource assessment and siting—a wider perspective; Riso—Contribution from the Department of Meteorology and Wind Energy to the EUWEC'96 Conference in Goeteborg, Sweden, Larsen GC editor, Riso National Laboratory, Roskilde, Denmark, August 1996, pp. 19–22.
- [140] Lewin B. CO₂-Emission von Energiesystemen zur Stromerzeugung unter Berücksichtigung der Energiewandlungsketten; Ph.D. thesis, Fachbereich 16, Bergbau und Geowissenschaften, Technical University Berlin, Germany, 1993.
- [141] Larsson, Å., Guidelines for grid connection of wind turbines, published in conference proceedings CIREN 1–4 June 1999, Nice, France 1999.
- [142] Larsson Å. The power quality of wind turbines. Ph.D. thesis, Dept. of Electrical Power Engineering at Chalmers University of Technology, Göteborg, Sweden, 2000.

- [143] Manwell JF, McGowan JG. Recent renewable energy driven desalination system research and development in North America. *Desalination* 1994;94(3):229–41.
- [144] Matthies H, Garrad AD. Study of offshore wind energy in the EC. Co-funded by the Commission of the European Communities (CEC) in the framework of the JOULE I programme under contract no. JOUR-0072, published by Verlag Natürliche Energie, Brekendorf, Germany, 1995. For an extract of the book see also: <http://www.germanlloyd.de/Activities/Wind/exsum/index.html>.
- [145] Mengelkamp H-T. Boundary layer structure over an inhomogeneous surface: simulation with a non-hydrostatic mesoscale model. *Boundary-Layer Meteorology* 1991;57:323–41.
- [146] Mengelkamp H-T, Kapitza H, Pflueger U. Statistical-dynamical downscaling of wind climatologies. *Journal of Wind Engineering and Industrial Aerodynamics*, June 1997;67–68:449–457.
- [147] Mengelkamp H-T. On the energy output estimation of wind turbines. *International Journal of Research* 1988;12:113–23.
- [148] Mitchell CR. Renewable generation—success story? In: Surrey J, editor. *The British electricity experiment—privatization: the record, the issues, the lessons*, London: Science Policy Research Unit Sussex University & Earthscan; 1996. p. 164–84.
- [149] Montavon C, Alexandrou C, Hertig J-A. Wind potential evaluation over complex terrain by means of a three-dimensional atmospheric numerical model. *Proceedings 1996 European Wind Energy Conference*, 20–24 May 1996, Goeteborg, Sweden, pp. 526–529.
- [150] Nath C, Quarton D. Chancen und Grenzen von Windenergieanlagen über 3 Megawatt—Eine Grenze zeichnet sich noch nicht ab. *Erneuerbare Energien* 1999;9(9):42–6.
- [151] National Renewable Energy Laboratory: <http://www.nrel.gov/international/tools/HOMER/homer.html>.
- [152] Nielsen TS, Joensen A, Madsen H, Landberg L, Giebel G. A new reference for wind power forecasting. *Wind Energy* 1999;1(1):29–34.
- [153] Nørgaard P, Lundsager P. A power quality framework for wind power applications. In: 1996 European Union wind energy conference. *Proceedings, EWEC '96*, Göteborg (SE), 20–24 May 1996. Zervos A, Ehmann H, Helm P (eds.), (H.S. Stephens & Associates, Bedford, 1996) p. 451–454.
- [154] Pedersen J, Eriksen PB, Mortensen P. Present and future integration of large-scale wind power into Eltra's power system. In: *Proceedings of the European Wind Energy Conference*, Copenhagen, Denmark, 2–6 July 2001, pp. 153–156.
- [155] Petersen EL, Mortensen NG, Landberg L. Measurements and modelling in complex terrain. Riso—Contribution from the Department of Meteorology and Wind Energy to the EUWEC'96 Conference in Goeteborg, Sweden, Larsen GC, editor, Riso National Laboratory, Roskilde, Denmark, August 1996, pp.11–14.
- [156] Petersen EL. The new European wind atlas method. Riso—Contribution from the Department of Meteorology and Wind Energy to the EUWEC'96 Conference in Goeteborg, Sweden, Larsen GC, editor, Riso National Laboratory, Roskilde, Denmark, August 1996, pp. 9–10.
- [157] Petersen EL, Mortensen NG, Landberg L, Højstrup J, Frank HP. Wind power meteorology, Part I: climate and turbulence. *Wind Energy* 1998;1(S1):25–45.
- [158] Petersen EL, Mortensen NG, Landberg L, Højstrup J, Frank HP. Wind power meteorology, Part II: siting and models. *Wind Energy* 1998;1(2):55–72.
- [159] Office of Electricity Regulation, UK. Fifth Renewable Order for England and Wales, September 1998, available at: <http://www.open.gov.uk/offer/offerhm.htm>.
- [160] Quarton DC. The evolution of wind turbine design analysis—a twenty year progress review. *Wind Energy* 1998;1(S1):5–24.
- [161] Rahal Z, Infield DG. Wind powered stand alone desalination. In: *Proceedings of the European Wind Energy Conference*, Dublin, Ireland, October 1997; also available at: <http://info.lboro.ac.uk/departments/el/research/crest/publicitn.html>.
- [162] Rahal Z, Infield DG. Computer modelling of a large scale stand alone wind-powered desalination plant. In: *Proceedings of the British Wind Energy Conference*, Stirling, UK, August 1997, also available at: <http://info.lboro.ac.uk/departments/el/research/crest/publicitn.html>
- [163] Rathmann O, Mortensen NG, Landberg L, Bowen A. Assessing the accuracy of WASP in non-simple terrain. *Proceedings of the 1996 Eighteenth BWEA (British Wind Energy Association) Conference*, pp. 413–418.

- [164] Cost optimisation of large-scale offshore wind farms. Riso National Laboratory, SK Power Company, Elkraft, National Wind Power, Nellesman Nielsen & Rauschenberger, Universidad Politecnica de Madrid, Stadtwerke Rostock, EU Joule III Project JOR3-CT95-0089, 1999.
- [165] Rodriguez-Girones PJ et al. Experience on desalination with renewable energy sources—EURORED project. University De Las Palmas De Gran Canaria, 1996.
- [166] Rosser, M. 70% penetration of wind energy into a rural grid—2.4 MW of wind capacity interconnected with a 14 MW diesel power station. In: Proceedings of the Wind Energy Workshop 1997, Asia Pacific Wind Energy Centre, Centre for Electrical Power Engineering, Monash University, Calyton, Australia.
- [167] Sagrillo, M. Apple & Oranges. Home Power no. 65, June/July 1998, USA, available at: <http://www.humboldt1.com/~michael.welch/apples.pdf>.
- [168] Santjer F, Gerdes G. Netrückwirkungen, verursacht durch den Betrieb von Windkraftanlagen am Netz (Grid interference caused by grid connected wind energy converters). In: DEWI Magazin, no. 5, August 1994, published by German Wind Energy Institute (Deutsches Windenergie-Institute), Wilhelmshaven, Germany.
- [169] Schleisner L. Life cycle assessment of a wind farm and related externalities. *Renewable Energy* 2000;20:279–88.
- [170] Schlez W. Voltage fluctuations caused by groups of wind turbines, Ph.D. thesis, Loughborough University, UK, 2000.
- [171] Shell International Petroleum Company. The evolution of the world's energy system 1860–2060. In: Conference Proceedings: "Energy technologies to reduce CO₂-emissions in Europe: prospects, competition, synergy". International Energy Agency, Paris, 1994, pp. 85–113.
- [172] Shepherd DG. Historical development of the windmill. In: Wind turbine technology. New York: SAME Press; 1994.
- [173] Siegfriedsen S, Böhmeke G. Multibrid technology—a significant step to multi-megawatt wind turbines. *Wind Energy* 1998;1(2):89–100.
- [174] Snel H. Review of the present status of rotor aerodynamics. *Wind Energy* 1998;1(S1):46–69.
- [175] Søbrink KH, Sørensen PL, Christensen P, Andersen N, Eriksson K, Holmberg P. DC feeder for connection of a wind farm. Cigré Symposium, Kuala Lumpur, Malaysia, September 1999.
- [176] Søbrink KH, Sørensen PL, Joncquel E, Woodford D. Feasibility study regarding grid integration of a 160 MW offshore wind farm using VSC transmission. In: Proceedings of the European Wind Energy Conference, Copenhagen, Denmark, 2–6 July 2001, pp. 56–59.
- [177] Söder L. Wind energy impact on the energy reliability of a hydro-thermal power system in a deregulated market. 13th Power Systems Computation Conference, June 28–July 2, 1999, Trondheim, Norway.
- [178] Söder L. The value of wind power for an owner of a local distribution network. Proceedings 15th International Conference on Electricity Distribution CIRED'99, June 1–4, 1999, Nice, France.
- [179] Sørensen MP. Learning curve: how are new energy technology costs reduced over time? Report of an IEA Workshop: Energy Technology Availability to Mitigate Future Greenhouse Gas Emissions, International Energy Agency, Paris 1997; see also: <http://www.iea.org/pubs/free/techav/toc.htm>.
- [180] Sørensen P, Unnikrishnan AK, Mathew SA. Wind farms connected to weak grids in India. *Wind Energy* 2001;3(3):137–49.
- [181] Stampa A. Synchronisation von netzgekoppelten Windenergieanlagen in einem Windpark (Synchronism of grid connected wind energy converters in a wind farm). DEWI Magazin, no. 7, August 1995, published by German Wind Energy Institute (Deutsches Windenergie-Institute), Wilhelmshaven, Germany.
- [182] Stiesdal H, Kruse H. 10 Years with arctic modifications—a manufacturer's experience. Denmark: Bonus Energy A/S, 1999.
- [183] Thresher RW, Dodge DM. Trends in the evolution of wind turbine generator configurations and systems. *Wind Energy* 1998;1(S1):70–85.
- [184] Van Bussel G, Schöntag C. Operation and maintenance aspects of large offshore windfarms. Proceedings of the European Wind Energy Conference in Dublin, Ireland, October 1997; also available at: <http://www.ct.tudelft.nl/windenergy/publicat.htm#IPp99>.
- [185] Van Bussel G. Power augmentation principles for wind turbines. Delft University of Technology,

- Institute for Wind Energy, the Netherlands, 1998; available at: <http://www.ct.tudelft.nl/windenergy/papers/augment/contents.htm>
- [186] Van Lieshout P. Accurate wind measurements and analysis for successful wind farm project development in New Zealand. In: Proceedings of the New Zealand Wind Energy Conference, 30 June, Wellington, New Zealand, 1997.
- [187] Van Wijk AJM, Coelingh JP. Wind potential in the OECD countries. University of Utrecht, December 1993.
- [188] University of Massachusetts: <http://www.ecs.umass.edu/mie/labs/rerl/hy2/demo/demo.htm>
- [189] Proceedings of the European Wind Energy Conference (EWEC), hosted by the Irish Wind Energy Association on behalf of the European Wind Energy Association, the European Wind Energy Conference, University College Dublin, Dublin, Watson R. editor, 1997.
- [190] Western Power (2001): see <http://www.denhamwinddiesel.com/> or <http://www.westernpower.com.au/our—environment/renewable—energy/wind/denham.html>.
- [191] Wiese A, Heil O. Methodik und beispielhafte Ergebnisse eines neuen Modelles fuer Windpotentialanalysen im komplexen Gelaende. Proceedings of the 3rd Deutsche Windenergie-Konferenz, 23–24 October 1996, in Wilhelmshaven, Germany, pp. 338–341.
- [192] Ackermann, Thomas, editor. Proceedings of the Third International Workshop on Transmission Networks for Offshore Wind Farms, April 2002, Royal Institute of Technology, Electric Power Systems, Stockholm, Sweden.
- [193] Sørensen P, Hansen AD, Janosi L, Bech J, Bak-Jensen B. Simulation of interaction between wind farm and power system. Risø National Laboratory, Report Nr.: Riso-R-1281 (EN), December 2001, available at: <http://www.risoe.dk/rispubl/VEA/ris-r-1281.htm>.
- [194] Lundsager Per, Bindner Henrik, Clausen Niels-Erik, Frandsen Sten, Hansen Lars Henrik, Hansen Jens Carsten. Isolated Systems with Wind Power Main Report. Risø National Laboratory, Report Nr.: Riso-R-1256 (EN), June 2001, available at: <http://www.risoe.dk/rispubl/VEA/ris-r-1256.htm>.
- [195] Hansen Lars Henrik, Lundsager Per. Review of Relevant Studies of Isolated Systems. Risø National Laboratory, Report Nr.: Riso-R-1109 (EN), December 2000, available at: <http://www.risoe.dk/rispubl/VEA/ris-r-1109.htm>.
- [196] Bindner Henrik. Power Control for Wind Turbines in Weak Grids: Project summary. Risø National Laboratory, Report Nr.: Riso-R-1117 (EN), March 1999, available at: <http://www.risoe.dk/rispubl/VEA/ris-r-1117.htm>.



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